

Source	Data / Information	Period of Record	Format
Soquel Creek Water District	Water Levels - Production Wells	6/90 - 9/03	MS Access file
		1973 - 1990	paper copies
	Water Levels - Monitoring Wells	1/83 - 3/02	MS Access file
	Groundwater Production - monthly by well - annual totals	11/83 - 9/03	MS Access file
		1966 - 1983	paper copy
	Well Information (status, elevation, depth, construction, coordinates)	N/A	MS Access file
	Production well geophysical logs and pump-test data	1965 - 2001	paper copies
	Water Quality Indicators - All Wells (TDS, Chloride, NO ₃)	9/73 - 10/03	MS Access file
	General Mineral Water Quality - Production Wells - Monitoring Wells	1942 - 2003	paper copies
		1995 - 2003	
	Main Street Well aquifer test data	5/91	paper copies
	Opal Cliffs well water levels monitored during Garnet well pilot injection test	5/00	
	Santa Cruz County GIS layers	8/03 version	ArcView
Linsley, Kraeger Associates	Mean daily stream discharge for 2 gages on upper branches of Soquel Creek	9/83 - present	electronic data files
	Daily precipitation for 2 gages	11/83 - present	
City of Santa Cruz Water Department	Water Levels - Production Wells	1979 - 2003	MS Excel files
	Water Levels - Monitoring Wells	1989 - 2004	
	Groundwater Production - by well	1972 - 2002	
	General Mineral Water Quality - Production Wells	7/70 - 2/03	MS Access files
	Water Quality Indicators - Monitoring Wells (Cl, EC, pH)	9/91 - 1/02	
Central Water District	Water Levels - Production Wells	1993 - 2004	MS Excel files
	Groundwater Production - by well	1986 - 2002	
USGS	Groundwater Levels - various wells	1965 - 1985	electronic data files from web site
	Mean daily streamflow for: Soquel Creek at Soquel Soquel Creek near Soquel West Branch Soquel Creek Branciforte Creek Aptos Creek at and near Aptos	5/51 - present	
		10/68 - 9/72	
		10/58 - 10/72	
		4/52 - 9/68	
		10/58 - 9/85	
	Streamflow Water Quality	1952 - 1977	
Santa Cruz County Environmental Health Services Department	Water level monitoring data contained in reports for 5 remediation sites	1988 - 2003	paper copies
NOAA, DWR, and others	Precipitation records: various stations	1867 - pres.	electronic data files and paper copies

Table 1-1
Summary of Available Data
(other than data provided in referenced reports)

Name	Alternate Names	State Well Number	Dist. Serv. Area	Production Capacity (gpm)	Gnd. Sfc. (ft msl)	Ref. Point	Stratigraphic Unit	Year Drilled	E-Log	Diam. (in)	Drilled	Completed Depth	Sanitary Seal (ft bgs)	Gravel Pack		Perforated/Screened Intervals							
														Top	Bot.	Range		Individual Intervals					Sum (ft)
																Top	Bot-tom	Top	Bot-tom	Top-Bot	(ft bgs)		
Active Wells																							
Main Street		11S/1W-10K	1	1,450	54	54	Tu/AA	1986	X	16/12	675	656	60	60	675	232	652	-179	-599	420	232-246, 280-376, 424-448, 472-496, 544-652	266	
Garnet	Opal 5	11S/1W-15?	1	700	81	81	A	1995	X	12	310	300	75	75	310	164	290	-83	-209	113	164-177, 190-290	113	
Rosedale		11S/1W-10J1	1	600	131	131	AA/A	1983	X	12	595	570	60	60	570	210	560	-79	-429	350	210-240, 266-310, 324-336, 350-400, 438-494, 530-560	222	
Monterey	Airport, Capitola Airport	11S/1W-11N1	1	400	113	113	A	1950		10	698	398				240	391	-127	-278	151	240-391	151	
Tannery II	Tannery	11S/1W-11L3?	1	530	123	123	A	2001	X	16	643	620	310	310	643	385	605	-262	-482	220	385-605	220	
Estates		11S/1W-12P	2	1,000	144	144	A/BC	1985	X	16/12	950	930	60	60	950	305	920	-161	-776	615	305-390, 440-510, 660-920	415	
Madeline 2			2	250	192		BC	1984	X	16	700	680	60	60	680	480	670	-288	-478	190	480-570, 600-670	160	
Ledyard		11S/1E-18D	2	300	190	190	BC	1985	X	12	880	880	60	60	880	640	850	-450	-660	210	640-850	210	
T. Hopkins	Hopkins	11S/1E-18F	2	350	120	120	DEF	1989		16	610	600	50	50	610	240	585	-120	-465	345	240-300, 340-380, 400-525, 535-545, 565-585	255	
Aptos Creek		11S/1E-18F1	2	500	26	26	BC/DEF	1965	X	12	725	713	88	88	713	243	713	-217	-687	470	243-713	470	
Country Club	Berry Farm, Reiter	11S/1E-20G1	3	350	197	197	F/Qa	1953		12	495	495	?	?	?	254	495	-57	-298	241	254-302, 326-350, 374-398, 422-495	169	
Bonita		11S/1E-21E1	3	900	231	231	F/Qa	1983	X	16/12	760	740	60	60	740	330	728	-99	-497	398	330-364, 380-410, 442-486, 518-542, 560-580, 600-634, 666-728	248	
Seascape		11S/1E-28D1	3	900	177	177	F/Qa	1970	(x)	16/10	810	550	54	54	550	310	550	-133	-373	240	310-340, 370-390, 410-440, 530-550	100	
San Andreas		11S/1E-21L	3	1,100	165	165	F/Qa	1991		16	880	630	65	65	640	268	610	-104	-446	342	268-348, 394-454, 510-610	240	
Sells		11S/1E-28R3	4	470	111	111	F/Qa	1983	X	16/12	445	440	120	120	440	200	430	-89	-319	230	200-260, 300-340, 410-430	120	
Altivo		11S/1E-28R4	4	620	166	166	F/Qa	1979	(x)	14/8	510	480	60	60	500	320	470	-154	-304	150	320-350, 385-425, 440-470	100	
Offline Wells																							
Opal 4	Opal Cliff	11S/1W-15?	1		81	81	A	1980			320	300	200	200	300	210	290	-129	-209	80	210-290	80	
Maplethorpe		11S/1W-11L1	1	350	135	135	A	1965	(x)	12		628	68			368	628	-233	-493	260	368-628	260	
Tannery		11S/1W-11L2	1	670	124	124	A	1970		14		614	60			340	600	-216	-476	260	340-600	260	
Madeline 1		11S/1W-12K1	2	460	192		A/BC	1972		16	1020	1020	60	60	1020	460	1000	-268	-808	540	460-690, 820-1000	410	
Aptos Jr. High School	Aptos, Aptos School, Aptos Reservoir, Old Aptos, at Monroe Ave, Rio Del Mar 1, Valentia, Luis Ranch?	11S/1E-17F1	3	390	210	210	F/Qa	1927		12 to 200'		460				200	460	10	-250	260	200-460 (uncased)	260	
Destroyed Wells																							
Opal 1	Opal	11S/1W-15L1	1	320	81	81	A	1930		10		211				109	211	-28	-130	102	109-211	102	
Opal 2			1																				
Opal 3	Opal Cliff 3	11S/1W-15L2	1	270	81	81	A	1954		12		256				184	256	-103	-175	72	184-256	72	
Rosedale 1	Soquel, Grove Ranch		1		135		A	1952		10		250				160	250	-25	-115	90	160-250 ?		
Maplethorpe 1?			1				A(&?)	1956															
Seacliff 2	at Soquel Dr	11S/1W-12Q1	2		170		EF	1949		12	400	350				140	350	30	-180	210	140-350 ?		
Seacliff 3	at Mesa Dr	11S/1E-12J1	2		302		EF	1926		14	600	515				360	515	-58	-213	155	360-515 ?		
Hillcrest	Seacliff 1, at Mar Vista, Railroad	11S/1W-13G1	2	190	145	145	EF	1923		10		330				200	330	-55	-185	130	200-330 or 340-585??	130	
State Park Dr	Seacliff	11S/1W-13A1	2		150		EF	1959		12	215					126	215	24	-65	89	126-215 ?		
Seacliff 4	Seacliff, at Center, Foster, Subdivision 8	11S/1W-18E1	2		111	111	EF	1935		10		300				140	289	-29	-178	149	140-289	149	
Palmer	at Dorsey, Rio Del Mar 2	11S/1E-17M1	3	180	188		F/Qa	1953		10		500				216	500	-28	-312	284	216-500 ?	160	
Cliff		11S/1E-20E1	3		63	63	F	1961		12	508	400	135			194	394	-131	-331	200	194-394	200	
La Selva1	LSB 1	11S/1E-28R1	4		120		Qa	1935		12		355				345	355	-225	-235	10	345-355	10	
La Selva2	LSB 2	11S/1E-28R2	4		130		Qa	1960		12		250				345	355	-215	-225	10	345-355	10	

italics = from Hickey, 1968

Within groups, listed in order from west to east as projected onto line of section shown in Figure 1-2.

Approximate production capacities based on range reported by LSCE (1994, 1999) and SCWD "Existing Water System Schematic Profile" (2000).

(x) indicates e-log reportedly exists, but was not seen as part of this review

Table 1-2
Soquel Creek Water District Production Wells

Well Cluster Name	Year Installed	State Well No.	Ref. Point (ft msl)	Total Depth		Well Label	Aquifer Unit*	Screened Interval				Gravel Pack			
								Top	Bot.	Top	Bot.	Top	Bot.		
								(ft bgs)		(ft msl)		(ft bgs)			
SC-1 Prospect Ave	1983	11S/1W-15P	72	320	-248	A	A	113	320	-40	-248	109	320		
SC-3 Escalona Dr	1983	11S/1W-14E	97	510	-413	A	A	278	510	-180	-413	270	510		
						B	B	113	240	-16	-143	113	240		
						C	C	52	94	45	3	52	95		
SC-5 New Brighton State Beach	1983	11S/1W-14B	120	765	-645	A	A	520	765	-400	-645	500	765		
						B	B	306	475	-186	-355	300	480		
						C	C	215	280	-95	-160	210	284		
						D	D	80	190	40	-70	75	190		
SC-8 Aptos Creek State Beach	1983	11S/1E-18N	11	1,100	-1,089	E	E	20	44	100	76	20	45		
						A	A	825	1,100	-814	-1,089	810	1,100		
						B	B	611	780	-600	-769	600	780		
						C	C	517	580	-506	-569	510	580		
						D	D	363	490	-352	-479	355	490		
SC-9 Seacliff Beach	1983	11S/1W-13F	13	900	-887	E	E	230	336	-219	-325	220	336		
						F	F	20	200	-9	-189	20	200		
						A	A	625	900	-612	-887	600	900		
						B	B	406	575	-393	-562	400	590		
						C	C	316	380	-303	-367	300	380		
SC-10 Cherryvale	1983	11S/1W-3B	86	436	-350	D	D	184	290	-171	-277	170	290		
						E	E	25	140	-12	-127	25	140		
						A	A	30	173	56	-87	280	440		
						AA	AA	296	436	-210	-350	25	175		
SC-11 Porter Gulch	1983		520	1,350	-830	A	AA	900	1,000	-380	-480	50	1,350		
						B	B	500	600	20	-80				
						C	C	380	460	140	60				
						D	D	200	300	320	220				
SC-13, Opal	1980	11S/1W-15	81	820	-739	A	AA/A	760	770	-679	-689	451	820		
SC-14 Madeline	1984	11S/1W-12K	192	1,140	-948	A	A	819	840	-627	-648	810	1,140		
								959	990	-767	-798				
								1,019	1,040	-827	-848				
								1,079	1,100	-887	-908				
						B	B	620	640	-428	-448	590	800		
								660	680	-468	-488				
C	C	460	480	-268	-288	50	580								
		500	520	-308	-328										
SC-16 Estates Dr	1985	11S/1W-12P	143	980	-837	A	A/B	660	970	-517	-827				
						B	C/D	305	465	-162	-322				
SC-17 Ledyard Way	1985	11S/1E-18D	187	1,240	-1,053	A	A	1,000	1,210	-813	-1,023				
						B	B	640	840	-453	-653				
						C	C	430	550	-243	-363				
						D	D	210	350	-23	-163				
SC-18 Main St	1986		50	620	-570	A	AA	210	340	-160	-290	70	390		
						AA	Tu	550	620	-500	-570	410	620		
SC-A1 Cliff Dr	1986	11S/1E-20E	65	530	-465	A	F	500	520	-435	-455	420	540		
								460	470	-395	-405				
								375	395	-310	-330	220	400		
						B	F	260	280	-195	-215				
								C	F	170	190	-105	-125	165	200
SC-A2 Sumner	1986	11S/1E-29H	127	490	-363	D	F	100	120	-35	-55	60	150		
						A	F	460	480	-333	-353	455	650		
						B	F	420	440	-293	-313	330	445		
SC-A3 Playa & Vista	1986	11S/1E-33E	103	320	-217	C	Qa _U	140	160	-13	-33	50	310		
								A	Qa _L	290	310	-187	-207	285	330
								B	Qa _L	260	270	-157	-167	205	275
						C	Qa _U	230	250	-127	-147				
125	145	-22	-42	50	185										
SC-A4 Canon del Sol	1986	12S/1E-3C	186	550	-364			A	F	520	540	-334	-354	515	560
						B	F	480	500	-294	-314	440	505		
						C	Qa _L	390	410	-204	-224	270	420		
								290	310	-104	-124				
						D	Qa _U	220	240	-34	-54	50	250		
SC-A5 Seascape	1986	11S/1E-28D	175	680	-505	A	F	650	670	-475	-495	630	700		
						B	F	580	600	-405	-425	510	610		
						C	Qa _L	410	430	-235	-255	255	280		
								370	390	-195	-215				
								310	330	-135	-155				
						D	Qa _U	210	230	-35	-55	50	235		
Pleasure Point (City of Santa Cruz)	1988	11S/1W-21H	45	335	-290	A	AA	325	345	-280	-300	317	362		
						B	A	210	230	-165	-185	170	300		
						C	A	110	130	-65	-85	50	150		

*AA-F: Units of Purisima Formation

Qa-up and Qa-low: Upper and lower division of Aromas Sand:

Tu: undifferentiated older sandstone

Table 1-3
Soquel-Aptos Monitoring Wells

Name	State Well Number	Ground Surface	Ref. Point	Aquifer Unit	Year Drilled	Diam. (in)	Depth Drilled	Completed Depth	Sanitary Seal	Gravel Pack		Perforated/Screened Intervals							
										Top	Bot.	Range				Individual Intervals			
		Top	Bot-tom				Top	Bot-tom	Top-Bot					Sum (ft)					
City of Santa Cruz																			
Active Wells																			
Beltz 7	11S/1W-21B2	44	56	AA/A	1974	12/8	405	274	50	50	274	124	264	-80	-220	140	124-149,189-264	100	
Beltz 8	11S/1W-16R4?	42	48	A	1998	14	240	210	80	80	220	100	180	-58	-138	80	100-180	80	
Beltz 9	11S/1W-21B/G?	40	43	A	1998	14	240	230	90	90	240	110	200	-70	-160	90	110-200	90	
Inactive and Destroyed Wells																			
Beltz 1	11S/1W-21G1	20	20	A/B	rehab 1951			116				91	116	-71	-96	25	?	?	
Beltz 2	11S/1W-21G2	20	20	A	1963			125				73	125	-53	-105	52	?	?	
Beltz 3	11S/1W-21B1	55		A	1951	10		137				92						45	
Beltz 4	11S/1W-16Q1			A	1955, rehab 1977														
Beltz 4A	11S/1W-16Q?	55	61	A	1985			136				90	136	-35	-81	46		46	
Beltz 5				A	1956			125											
Beltz 6	11S/1W-16R3	42	48	A	1966	8	260	178	70	70	178	104	169	-62	-127	65	104-114,119-134,135-151,156-169	51	
Central Water District																			
CWD 1	11S/1E-4Q1	286	286		1952	10		248				90		196					
CWD 2								261										140	
CWD 3	11S/1E-4Q?		290					300											
CWD 4	11S/1E-17R		150																
CWD 5	11S/1E-4Q?		318					272											
CWD 6																			
CWD 7																			
CWD 8																			
CWD 9																			
CWD 10	11S/1E-17R		156																
CWD 11																			
CWD 12			172																

italics = from Hickey, 1968

Table 1-4
Other Soquel-Aptos Production Wells

Contact		Note	Depth (ft bgs)	Elev. (ft msl)	Thickness		Screened Intervals			Unit
Top	Bottom				Unit ^x	(ft)	(ft bgs)	% of Unit	% of Total	Contact Source
Garnet										
ground surface			0	81						
B	C				C					
A	B		82	-1	B				a,d	
AA	A		290	-209	A	208	164 - 177	54%	100%	
							190 - 290		a,d	
Tu	AA	>	420	-339	AA	130			a	
basement	Tu				Tu					
Main Street										
ground surface			0	54						
B	C	*	-255	310	C				c	
A	B	*	-65	120	B	190			c	
AA	A		170	-116	A	235			a,b,d	
Tp?	AA		390	-336	AA	220	232 - 246	50%	41%	
							280 - 376		a	
Tu	Tp?		535	-481	Tp?	145	424 - 448	33%	18%	
							472 - 496		a	
basement	Tu		668	-614	Tu	133	544 - 652	81%	41%	
Rosedale										
ground surface			0	131						
C	D				D					
B	C	*	-110	240	C				c	
A	B		140	-9	B	250			a,b,d	
AA	A		405	-274	A	265	210 ^ 400	51%	61%	
Tu	AA	>	660	-529	AA	255	438 ^ 560	34%	39%	
basement	Tu				Tu				a	
Maplethorpe										
ground surface			0	135						
C	D				D					
B	C		143	-8	C				b,f	
A	B		368	-233	B	225			b,f	
AA	A		620	-485	A	252	368 - 628	100%	100%	
Tu	AA	>	760	-625	AA	140			b	
basement	Tu				Tu				c	

Contact		Note	Depth (ft bgs)	Elev. (ft msl)	Thickness		Screened Intervals			Unit Contact Source
Top	Bottom				Unit ^x	(ft)	(ft bgs)	% of Unit	% of Total	
Monterey										
ground surface			0	113						
B	C				C					
A	B		225	-112	B					f
AA	A		480	-367	A	255	240 - 391	59%	100%	f
Tu	AA				AA					
basement	Tu				Tu					
Tannery II										
ground surface			0	123						
D	E				E					
C	D		43	80	D					
B	C		153	-30	C	110				a
A	B		378	-255	B	225				a
AA	A		609	-486	A	231	385 - 605	95%	100%	a
Tu	AA		790	-667	AA	181				a
basement	Tu	>	836	-713	Tu	46				a
Grove Ranch										
ground surface			0	110						
A	B				B					
AA	A		265	-155	A					b
Tu	AA		490	-380	AA	225				c
basement	Tu		720	-610	Tu	230				c

^xBold highlights which aquifer units are screened.

Service Area I wells (screened in Purisima units A and AA)

Table 2-1a
Interpreted Stratigraphic Contacts -- Production Wells
 See notes last page Table 2-1a

Contact		Note	Depth (ft bgs)	Elev. (ft msl)	Thickness		Screened Intervals			Unit
Top	Bottom				Unit ^x	(ft)	(ft bgs)	% of Unit	% of Total	Contact Source
Estates (SC-16)										
ground surface			0	144						
E	F	*	-10	154	F					f
D	E		140	4	E	150				a,d
C	D		300	-156	D	160				a,d
B	C		410	-266	C	110	305 - 390	77%	20%	a,d
A	B		650	-506	B	240	440 - 510	29%	17%	a,d
AA	A		925	-781	A	275	660 - 920	95%	63%	a,d
Tu	AA	>	1,100	-956	AA	175				a
basement	Tu				Tu					
Madeline (SC-14)										
ground surface			0	192						
E	F		178	14	F					a,b,d
D	E		320	-128	E	142				a,b,d
C	D		445	-253	D	125				a,b,d
B	C		565	-373	C	120	480 - 545	54%	41%	a,b,d
A	B		800	-608	B	235	545 - 570 600 - 670	40%	59%	a,b,d
AA	A		1,040	-848	A	240				a,b,d
Tu	AA	>	1,220	-1,030	AA	180				a
basement	Tu		1,435	-1,240	Tu					c
T. Hopkins										
ground surface			0	120						
E	F		380	-260	F	380	240 ^ 380	26%	39%	f
D	E		525	-405	E	145	400 - 525	86%	49%	f
C	D		624	-504	D	99	535 ^ 585	30%	12%	f
B	C				C					
basement	Tu				Tu					

Contact		Note	Depth (ft bgs)	Elev. (ft msl)	Thickness		Screened Intervals			Unit
Top	Bottom				Unit ^x	(ft)	(ft bgs)	% of Unit	% of Total	Contact Source
Aptos Creek										
ground surface			0	26						
E	F		305	-279	F	305	243 - 305	20%	13%	a
D	E		470	-444	E	165	305 - 470	100%	35%	a
C	D		590	-564	D	120	470 - 590	100%	26%	a
B	C	>	600	-574	C	10	590 - 713	37%	26%	a
A	B		926	-900	B					
AA	A				A					
Tu	AA				AA					
basement	Tu				Tu					
Ledyard (SC-17)										
ground surface			0	190						
E	F		335	-145	F	335				
D	E		515	-325	E	180				a
C	D		635	-445	D	120				a
B	C		750	-560	C	115	640 - 750	96%	52%	a
A	B		990	-800	B	240	750 - 850	42%	48%	a
AA	A	>	1,240	-1,050	A	250				a
Tu	AA				AA					
basement	Tu				Tu					

^xBold highlights which aquifer units are screened.

Service Area II wells (screened in Purisima units B, C, D, E)

Table 2-1a (continued)
Interpreted Stratigraphic Contacts -- Production Wells
 See notes last page Table 2-1a

Contact		Note	Depth (ft bgs)	Elev. (ft msl)	Thickness		Screened Intervals			Unit
Top	Bottom				Unit ^x	(ft)	(ft bgs)	% of Unit	% of Total	Contact Source
Country Club										
ground surface			0	197						
Qa-lower	Qa-upper		187	10	Qa _U	187			f	
F	Qa-lower		360	-163	Qa_L	173	254 ^ 350	42%	43%	f
E	F	>	495	-298	F	135	374 ^ 495	***	57%	a
D	E				E					
basement	Tu				Tu					
Bonita										
ground surface			0	231						
Qa-lower	Qa-upper		250	-19	Qa _U	250				
F	Qa-lower		415	-184	Qa_L	165	330 ^ 410	39%	26%	a
E	F	>	800	-569	F	385	442 ^ 728	***	74%	a
D	E				E					
basement	Tu				Tu					
San Andreas										
ground surface			0	165						
Qa-lower	Qa-upper		244	-79	Qa _U	244				f
F	Qa-lower		349	-184	Qa_L	105	268 - 348	76%	33%	f
E	F	>	880	-715	F	531	394 ^ 610	***	67%	a
D	E				E					
basement	Tu				Tu					

*** Bottom and thickness of unit are undefined.

Service Area III and IV wells (screened in Purisima Unit F and Aromas Sands)

Contact		Note	Depth (ft bgs)	Elev. (ft msl)	Thickness		Screened Intervals			Unit
Top	Bottom				Unit ^x	(ft)	(ft bgs)	% of Unit	% of Total	Contact Source
Seascape										
ground surface			0	177						
Qa-lower	Qa-upper		250	-73	Qa _U	250			f	
F	Qa-lower		362	-185	Qa _L	112	310 ^ 340	27%	30%	f
E	F	>	810	-633	F	448	370 ^ 550	***	70%	a
D	E				E					
basement	Tu				Tu					
Sells										
ground surface			0	111						
Qa-lower	Qa-upper		?							
F	Qa-lower		345	-234	Qa	345	200 ^ 340	29%	83%	a
E	F	>	747	-636	F	402	410 - 430	***	17%	a
D	E				E					
basement	Tu				Tu					
Altivo										
ground surface			0	166						
Qa-lower	Qa-upper		244	-78	Qa _U	244				f
F	Qa-lower		380	-214	Qa _L	136	320 - 350	22%	30%	f
E	F	>	510	-344	F	130	385 ^ 470	***	70%	a
D	E				E					
basement	Tu				Tu					

^xBold highlights which aquifer units are screened.

Table 2-1a (continued)
Interpreted Stratigraphic Contacts -- Production Wells
 See notes last page Table 2-1a

Contact		Note	Depth (ft bgs)	Elev. (ft msl)	Thickness		Screened Intervals			Unit Contact Source
Top	Bottom				Unit ^x	(ft)	(ft bgs)	% of Unit	% of Total	
Beltz 7 (test hole 2 E-log)										
ground surface			0	44						
B	C				C					
A	B	*	-65	110	B					f
AA	A		155	-111	A	220	124 - 149	11%	25%	a,d
Tp?	AA		360	-316	AA	205	189 - 264	37%	75%	a,d
Tu	Tp?	>	435	-391	Tp?	75				a,d
basement	Tu				Tu					
Beltz 6 and 8 (test hole 3 E-log)										
ground surface			0	42						
B	C				C					
A	B	*	-30	72	B		Beltz 6			f
AA	A		180	-138	A	210	104 ^ 169	31%	100%	a,d
							100 - 180	38%	100%	
Tp?	AA		375	-333	AA	195	Beltz 8			a,d
Tu	Tp?		500	-458	Tp?	125				a,d
basement	Tu	>	606	-564	Tu	106				a
Beltz 9 (test hole 1 E-log)										
ground surface			0	40						
B	C				C					
A	B	*	-10	50	B					f
AA	A		200	-160	A	210	110 - 200	43%	100%	a
Tp?	AA		360	-320	AA	160				a
Tu	Tp?	>	426	-386	Tp?	66				a
basement	Tu				Tu					

^xBold highlights which aquifer units are screened.

Beltz Wells (screened in Purisima Units A and AA)

Key to Units

Qa-upper Aromas Sands upper zone
 Qa-lower Aromas Sands lower zone
 AA - F Purisima units AA, A, B, C, D, E, and F
 Tp? Fine-grained zone below Purisima unit AA
 Tu Older Tertiary sandstone, possibly Santa Margarita or Lompico sandstone
 basement Granitic basement rock

Key to "Note" Symbols and Unit Abbreviations

** Ground surface elevation estimated.
 * Contact extrapolated above ground surface from available cross section.
 > Contact is below bottom of well log, thus contact depth is greater than value.
 ^ Spans multiple screened intervals.
 bgs below ground surface
 msl elevation relative to mean sea level
Italics indicate rough estimates (either because estimated ground surface or contact estimated from cross section).

Key to Sources

a Reviewed e-log.
 b Contact depth posted on LSCE cross section (1984).
 c Contact suggested by LSCE cross section (1984, 1987).
 d Contact indicated on draft cross sections by M. Cloud, Santa Cruz Co. FCWCD.
 e Thorup, 1981.
 f Estimated consistent with overall interpretation.

See Tables 1-1 through 1-3 for detailed well information.

Table 2-1a (continued)
Interpreted Stratigraphic Contacts -- Production Wells

Contact		Note	Depth (ft bgs)	Elev. (ft msl)	Thickness		Monitoring Well Label	Screened Interval		Unit Contact Source
Top	Bottom				Unit	(ft)		(ft bgs)	% of Unit	
SC-1										
ground surface			0	72						
E	F	*	-520	590	F					c
D	E	*	-370	440	E	150				c
C	D	*	-220	290	D	150				c
B	C	*	-110	180	C	110				c
A	B		114	-42	B	224	B	50 - 80	13%	a,b
AA	A		323	-251	A	209	A	113 - 320	99%	a,b
Tu	AA	>	520	-448	AA					a
basement	Tu		880	-810	Tu	557				c
SC-3										
ground surface			0	97						
E	F	*	-315	410	F					c
D	E	*	-155	250	E	160				c
C	D	*	-15	110	D	140				c
B	C		95	2	C	110	C	52 - 94	38%	a,b
A	B		280	-183	B	185	B	113 - 240	69%	a,b,d
AA	A		510	-413	A	230	A	278 - 510	101%	a,b,d
Tu	AA		700	-603	AA	190				a,d
basement	Tu		1,080	-980	Tu	380				c
SC-5										
ground surface			0	120						
E	F	*	-115	235	F					
D	E		40	80	E	155	E	20 - 44	55%	c
C	D		172	-52	D	132	D	80 - 190	83%	a,b,d
B	C		282	-162	C	110	C	215 - 280	59%	a,b,d
A	B		516	-396	B	234	B	306 - 475	72%	a,b,d
AA	A		768	-648	A	252	A	520 - 765	97%	a,b,d
Tu	AA	>	790	-670	AA					a
basement	Tu		1,290	-1,170	Tu	522				c
SC-8										
ground surface			0	11						
E	F		207	-196	F	>207	F	20 - 200	87%	a,b,d
D	E		363	-352	E	156	E	230 - 336	68%	a,b,d
C	D		480	-469	D	117	D	363 - 490	100%	a,b,d
B	C		590	-579	C	110	C	517 - 580	57%	a,b,d
A	B		830	-819	B	240	B	611 - 780	70%	a,b,d
AA	A	>	1,012	-1,001	A	182	A	825 - 1,100	100%	a
Tu	AA				AA					
basement	Tu		1,530	-1,520	Tu	518				c

Contact		Note	Depth (ft bgs)	Elev. (ft msl)	Thickness		Monitoring Well Label ^a	Screened Interval		Unit Contact Source
Top	Bottom				Unit ^b	(ft)		(ft bgs)	% of Unit	
SC-9										
ground surface			0	13						
E	F		15	-2	F					a,d
D	E		143	-130	E	128	E	25 - 140	90%	a,b,d
C	D		286	-273	D	143	D	184 - 290	71%	a,b,d
B	C		385	-372	C	99	C	316 - 380	65%	a,b,d
A	B		625	-612	B	240	B	406 - 575	70%	a,b,d
AA	A		905	-892	A	280	A	625 - 900	98%	a,b,d
Tu	AA	>	965	-952	AA	450				a
basement	Tu		1,355	-1,340	Tu					c
SC-10										
ground surface			0	86						
D	E				E					
C	D	*	-490	580	D					a,c
B	C				C					
A	B	*	-100	190	B	390				a,c
AA	A		173	-87	A	273	A	30 - 173	52%	a,b
Tu/Tp?	AA		425	-340	AA	252	AA	296 - 436	51%	a,c
basement	Tu/Tp?		648	-562	Tu/Tp?	223				a,b
SC-11										
ground surface		**	0	520						
E	F		68	452	F					a,b
D	E		218	302	E	150				a,b
C	D		372	148	D	154	D	200 - 300	65%	a,b
B	C		475	45	C	103	C	380 - 460	78%	a,c
A	B		749	-229	B	274	B	500 - 600	36%	a,b
AA	A		960	-440	A	211				a,b
Tu	AA		1,310	-790	AA	350	A	900 - 1,000	29%	a,c
basement	Tu		1,341	-821	Tu	31				a,b
SC-18										
ground surface			0	50						
B	C				C					based on Main Street well
A	B	*	-69	120	B					
AA	A		176	-126	A	245				
Tp?	AA		386	-336	AA	210	A	210 - 340	62%	
Tu	Tp?		541	-491	Tp?	155				
basement	Tu		664	-610	Tu	123	AA	550 - 620	57%	

^aBold highlights where aquifer unit and well label designations do not match.

Table 2-1b
Interpreted Stratigraphic Contacts -- Monitoring Wells
 See notes last page Table 2-1a

Contact		Note	Depth (ft bgs)	Elev. (ft msl)	Thickness		Monitoring Well Label ^a	Screened Interval		Unit Contact Source
Top	Bottom				Unit ^x	(ft)		(ft bgs)	% of Unit	
SC-A1										
ground surface			0	65						
F	Qa		65	0	Qa	65	d			
E	F		605	-540	F	540	D	100 - 120	100%	a,c
							C	170 - 190		
							B	260 - 280		
								375 - 395		
								A		
			500 - 520							
D	E		760	-695	E	155				c
A	B		1,250	-1,185	B	490				c
AA	A				A					
basement	Tu		1,850	-1,785	Tu	600				c
SC-A2										
ground surface			0	127						
Qa-lower	Qa-upper		170	-43	Qa _U	170	C	140 - 160	12%	a,c
F	Qa-lower		300	-173	Qa _L	130				a,c
E	F		935	-810	F	635	B	420 - 440	6%	c
							A	460 - 480		
D	E		1,100	-970	E	165				c
A	B		1,630	-1,500	B	530				c
AA	A				A					
basement	Tu		2,160	-2,030	Tu	530				c
SC-A3										
ground surface			0	103						
Qa-lower	Qa-upper		190	-87	Qa _U	190	C	125 - 145	11%	a,c
F	Qa-lower		320	-217	Qa _L	130	B	230 - 250	38%	a,c
								260 - 270		
										A
E	F		1,180	-1,080	F	860				c
D	E		1,360	-1,260	E	180				c
A	B		1,920	-1,820	B	560				c
AA	A				A					
basement	Tu		2,420	-2,320	Tu	500				c

Contact		Note	Depth (ft bgs)	Elev. (ft msl)	Thickness		Monitoring Well Label ^f	Screened Interval		Unit Contact Source
Top	Bottom				Unit ^x	(ft)		(ft bgs)	% of Unit	
SC-A4										
ground surface			0	186						
Qa-lower	Qa-upper		260	-74	Qa_U	260	D	220 - 240	8%	a,c
F	Qa-lower		420	-234	Qa_L	160	C	290 - 310	25%	a,c
								390 - 410		
E	F		1,265	-1,080	F	845	B	480 - 500	5%	c
							A	520 - 540		
D	E		1,430	-1,240	E	165				c
A	B		2,025	-1,840	B	595				c
AA	A				A					
basement	Tu		2,740	-2,550	Tu	715				c
SC-A5										
ground surface			0	175						
Qa-lower	Qa-upper		245	-70	Qa_U	245	D	210 - 230	8%	a,c
F	Qa-lower		360	-185	Qa_L	115	C	310 - 330	52%	a,c
								370 - 390		
								410 - 430		
							B	580 - 600	16%	c
							A	650 - 750		
D	E		1,285	-1,110	E	165				c
A	B		1,835	-1,660	B	550				c
AA	A				A					
basement	Tu		2,320	-2,145	Tu	485				c
Pleasure Point monitoring well										
ground surface			0	45						
B	C				C					
A	B		105	-60	B					a
AA	A		312	-267	A	207	C	110 - 130	19%	a
							B	210 - 230		
Tu	AA	>	420	-375	AA	108	A	325 - 345	19%	a
basement	Tu				Tu					

^aBold highlights where aquifer unit and well label designations do not match.

Table 2-1b (continued)
Interpreted Stratigraphic Contacts -- Monitoring Wells
 See notes last page Table 2-1a

Contact		Note	Depth (ft bgs)	Elev. (ft msl)	Thickness		Unit Contact Source
Top	Bottom				Unit	(ft)	
Opal test hole 1							
ground surface			0	81			
E	F	*	-550	630	F		c
D	E	*	-400	480	E	150	c
C	D	*	-260	340	D	140	c
B	C	*	-140	220	C	120	c
A	B		80	1	B	220	b
AA	A		280	-200	A	200	c
Tu	AA		540	-460	AA	260	c
basement	Tu		800	-720	Tu	260	c
O'Neill Ranch test hole							
ground surface		**	0	110			
A	B				B		
AA	A		110	0	A		a
Tp?	AA		420	-310	AA	310	a
Tu	Tp?		540	-430	Tp?	120	a
basement	Tu	>	570	-460	Tu	150	a
Monte Toyon							
ground surface		**	0	250			
E	F		495	-245	F		c
D	E		655	-405	E	160	c
C	D		828	-578	D	173	b
B	C		935	-685	C	107	c
A	B		1,222	-972	B	287	b
AA	A		1,475	-1,225	A	253	c
Tu	AA				AA		
basement	Tu		1,750	-1,500	Tu	275	e
SC-12							
ground surface		**	0	320			
E	F		1,110	-790	F		c
D	E		1,270	-950	E	160	c
C	D		1,392	-1,072	D	122	b
B	C		1,490	-1,170	C	98	c
A	B		1,752	-1,432	B	262	b
AA	A		2,020	-1,700	A	268	c
Tu	AA				AA		
basement	Tu	>	1,986	-1,670			b
			2,420	-2,100	Tu	400	c

Contact		Note	Depth (ft bgs)	Elev. (ft msl)	Thickness		Unit Contact Source
Top	Bottom				Unit	(ft)	
Thurber Lane North							
ground surface		**	0	360			
A	B				B		
AA	A		145	215	A		a,d
Tp?	AA		385	-25	AA	240	a,d
Tu	Tp?		517	-157	Tp?	132	a
basement	Tu		575	-215	Tu	58	a,d
Santa Cruz test hole 1							
ground surface			0	110			
C	D				D		
B	C	*	-300	410	C		c
A	B	*	-110	220	B	190	c
AA	A		150	-40	A	260	b
Tu	AA				AA		
basement	Tu		615	-505	Tu	465	b
Santa Cruz test hole 2							
ground surface			0	65			
E	F	*	-660	725	F		c
D	E	*	-500	565	E	160	c
C	D	*	-355	420	D	145	c
B	C	*	-230	295	C	125	c
A	B	*	-10	75	B	220	c
AA	A		185	-120	A	195	c
Tu	AA				AA		
basement	Tu		730	-665	Tu	545	b
Texaco-Pierce 1							
ground surface		**	0	235			
E	F		1,675	-1,440	F		c
D	E		1,810	-1,575	E	135	c
C	D		1,950	-1,715	D	140	c
B	C		2,070	-1,835	C	120	c
A	B		2,315	-2,080	B	245	c
AA	A				A		
Tu	AA				AA		
basement	Tu		2,600	-2,365	Tu	285	c

Table 2-1c
Intrpreted Stratigraphic Contacts -- Test Holes
 See notes last page Table 2-1a

Layer	Bot Top	Thurber Ln N			O'Neill Ranch			SC-10			Beltz 7			Beltz 9			Beltz 8			Main Street			Pleasure Point		
		bgs	msl	thick	bgs	msl	thick	bgs	msl	thick	bgs	msl	thick	bgs	msl	thick	bgs	msl	thick	bgs	msl	thick	bgs	msl	thick
	gs	0	360	-	0	110	-	0	86	-	0	44	-	0	40	-	0	42	-	0	54	-	0	45	-
1	Qa_u - Qa _L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
2	Qa_L - F	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
3	F - DEF	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
4	DEF - D	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
5	D - BC	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
6	BC - B	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
7	B - A	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
8	A - AA	145	215	145	110	0	110	175	-89	175	155	-111	155	200	-160	200	180	-138	180	170	-116	170	312	-267	-
9	AA - Tp	385	-25	240	420	-310	310	425	-339	250	362	-318	207	360	-320	160	374	-332	194	390	-336	220	-	-	-
10	Tp - Tu	517	-157	132	540	-430	120	-	-	-	-	-	-	-	-	-	-	-	-	535	-481	145	-	-	-
11	Tu - gr	575	-215	58	-	-	-	648	-562	223	-	-	-	-	-	-	-	-	-	668	-614	133	-	-	-

Layer	Bot Top	Garnet			Rosedale			SC-1			Monterey			SC-3			Maplethorpe			Tannery			SC-5		
		bgs	msl	thick	bgs	msl	thick	bgs	msl	thick	bgs	msl	thick	bgs	msl	thick	bgs	msl	thick	bgs	msl	thick	bgs	msl	thick
	gs	0	81	-	0	131	-	0	72	-	0	113	-	0	97	-	0	135	-	0	123	-	0	120	-
1	Qa_u - Qa _L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
2	Qa_L - F	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
3	F - DEF	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
4	DEF - D	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	93	27	-
5	D - BC	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	177	-57	84
6	BC - B	-	-	-	-	-	-	-	-	-	-	-	-	95	2	-	-	-	-	153	-30	153	378	-258	201
7	B - A	82	-1	-	140	-9	140	114	-42	-	240	-127	-	280	-183	185	368	-233	-	325	-202	172	516	-396	138
8	A - AA	290	-209	208	405	-274	265	323	-251	209	488	-375	248	510	-413	230	620	-485	252	609	-486	284	768	-648	252
9	AA - Tp	-	-	-	-	-	-	-	-	-	-	-	-	700	-603	190	-	-	-	-	-	-	-	-	-
10	Tp - Tu	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	790	-667	181	-	-	-
11	Tu - gr	-	-	-	-	-	-	880	-808	557	-	-	-	907	-810	207	-	-	-	-	-	-	-	-	-

Layer	Bot Top	Estates			Madeline			SC-9			Seacliff 2			Ledyard			SC-8			T. Hopkins			Aptos Creek		
		bgs	msl	thick	bgs	msl	thick	bgs	msl	thick	bgs	msl	thick	bgs	msl	thick	bgs	msl	thick	bgs	msl	thick	bgs	msl	thick
	gs	0	144	-	0	192	-	0	13	-	0	170	-	0	190	-	0	11	-	0	120	-	0	26	-
1	Qa_u - Qa _L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
2	Qa_L - F	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
3	F - DEF	-	-	-	20	172	-	-	-	-	140	30	-	210	-20	210	50	-39	-	240	-120	240	160	-134	160
4	DEF - D	210	-66	-	345	-153	325	212	-199	-	-	-	-	551	-361	341	415	-404	365	535	-415	295	510	-484	350
5	D - BC	300	-156	90	443	-251	98	273	-260	61	-	-	-	635	-445	84	475	-464	60	-	-	-	590	-564	80
6	BC - B	515	-371	215	670	-478	227	480	-467	207	-	-	-	848	-658	213	665	-654	190	-	-	-	-	-	-
7	B - A	650	-506	135	803	-611	133	626	-613	146	-	-	-	990	-800	142	830	-819	165	-	-	-	-	-	-
8	A - AA	925	-781	275	1080	-888	277	905	-892	279	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
9	AA - Tp	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
10	Tp - Tu	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
11	Tu - gr	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Layer	Bot Top	SC-A1			Country Club			Bonita			SC-A2			SC-A5			Seascape			San Andreas			SC-A3		
		bgs	msl	thick	bgs	msl	thick	bgs	msl	thick	bgs	msl	thick	bgs	msl	thick	bgs	msl	thick	bgs	msl	thick	bgs	msl	thick
	gs	0	65	-	0	197	-	0	231	-	0	127	-	0	175	-	0	177	-	0	165	-	0	103	-
1	Qa_u - Qa _L	-	-	-	187	10	187	250	-19	250	170	-43	170	245	-70	245	250	-73	250	244	-79	244	190	-87	190
2	Qa_L - F	65	0	65	360	-163	173	415	-184	165	300	-173	130	360	-185	115	362	-185	112	349	-184	105	320	-217	130
3	F - DEF	460	-395	395	-	-	-	908	-677	493	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
4	DEF - D	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
5	D - BC	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
6	BC - B	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
7	B - A	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
8	A - AA	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
9	AA - Tp	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
10	Tp - Tu	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
11	Tu - gr	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Layer	Bot Top	Sells			Altivo			SC-A4		
		bgs	msl	thick	bgs	msl	thick	bgs	msl	thick
	gs	0	111	-	0	166	-	0	186	-
1	Qa_u - Qa _L	-	-	-	244	-78	244	260	-74	260
2	Qa_L - F	345	-234	-	380	-214	136	420	-234	160
3	F - DEF	-	-	-	-	-	-	-	-	-
4	DEF - D	-	-	-	-	-	-	-	-	-
5	D - BC	-	-	-	-	-	-	-	-	-
6	BC - B	-	-	-	-	-	-	-	-	-
7	B - A	-	-	-	-	-	-	-	-	-
8	A - AA	-	-	-	-	-	-	-	-	-
9	AA - Tp	-	-	-	-	-	-	-	-	-
10	Tp - Tu	-	-	-	-	-	-	-	-	-
11	Tu - gr	-	-	-	-	-	-	-	-	-

Table 2-2
Interpreted Hydrostratigraphic Contacts

Listed from west to east as projected onto line of section shown in Figure 1-2
 Bold in 2nd column indicates layers for which thicknesses and well screens correspond.
 Shading indicates zone screened/perforated by production well.

Author	Test Date	Assumed		Obs. Well	Actual Aquifer Zone*	Method	Type	Transmissivity (T) (ft ² /day)	Hydraulic Conductivity (K) (ft/day)	Solution Coefficients		K _V or K' (ft/day)	K _V :K _H or K'/K Ratio	Storativity (S)	Specific Yield (S _y)	Comments
		Aquifer Thickness (b) (ft)	Aquitar-d Thickness (b') (ft)							r/B or β	B or S/S'					
LSCE, 1991	Jul-86	400	-	Main St	Tu/AA	Cooper-Jacob	C	4,260	10.7	-	-	-	-	-	-	
				SC-18AA	Tu			4,390	11.0	-	-	-	-	0.00082	-	
				SC-18A	AA			4,590	11.5	-	-	-	-	0.00433	-	
	May-91		unspecified		unspecified	?	3,880 - 4,540	9.7-11.4	-	-	-	-	0.0033	-		
LSCE, 1995	May-91	400	100	Main St	Tu/AA	Theis	C	4,270	10.7	-	-	-	-	3.9E-05	-	
				SC-18AA	Tu	Theis	C	3,750	9.4	-	-	-	-	0.00125	-	
				SC-18A	AA	Hantush-Jacob	L	3,790	9.5	0.04	980	0.4	0.042	0.0066	-	
Todd, 2001	May-91	400	-	unspecified		unspecified	?	4,010	10	-	-	-	-	0.0008	-	
Johnson, 2001	May-91	400	100	Main St	Tu/AA	Theis	C	4,050	10.1	-	-	-	-	-	-	
						Hantush-Jacob	L	3,975	9.9	-	-	-	-	-	-	
				SC-18AA	Tu	Cooper-Jacob	C	3,735	9.3	-	-	-	-	0.0013	-	
						Theis	C	3,560	8.9	-	-	-	-	0.002	-	
						Hantush-Jacob	L	3,415	8.5	0.0066	5,870	0.01	0.001	0.0025	-	
						Hantush	L	3,400	8.5	0.00073	1	0.002	0.0002	0.0025	-	
						Neuman	UC	3,400	8.5	0.0001	-	0.094	0.01	0.0025	0.0025	
				SC-18A	AA	Cooper-Jacob	C	4,475	11	-	-	-	-	0.0045	-	
						Theis	C	4,600	12	-	-	-	-	0.0057	-	
						Hantush-Jacob	L	4,200	10.5	0.035	1,110	0.34	0.03	0.0068	-	
						Hantush	L	3,700	9.3	0.024	1	2.2	0.24	0.0063	-	
						Neuman	UC	3,100	7.8	0.0001	-	0.086	0.01	0.01	0.056	
this report	May-91	400	-	Main St	Tu/AA	S _c x 2000	C	3,700	9.3	-	-	-	-	-	-	s=53 ft, S _c =14 gpm/ft
		600	30	SC-18AA	Tu	Hantush-Jacob Theis (same S & T)	L C	3,590	6.0	0.01	3,900	0.007	0.00059	0.0015	-	See Figure 3-2
		400	100						9.0			0.02				
		300	200						12.0			0.05	0.008			
		600	30	SC-18A	AA	Hantush-Jacob	L	3,730	6.2	0.04	975	0.12	0.01	0.007	-	See Figure 3-3
		400	100						9.3			0.4				
		300	200						12.4			0.8	0.13			
		600	30	SC-10AA	AA	Hantush-Jacob	L	3,765	6.3	0.95	7,163	0.002	0.0002	0.00012	-	SC-10AA s ~2.5 ft SC-10A s <0.5 ft See Figure 3-4
		400	100						9.4			0.007				
		300	200						12.6			0.01	0.002			
		600	30			Hantush	L	4,455	7.4	0.3879	1	0.01	0.0005	6.5E-05	-	
		400	100						11.1			0.02				
300	200	14.9	0.05						0.01							
Average									3,900			9.8	n/a			
Minimum								3,100	6.0	-	-	0.002	0.00018	4E-5	0.0025	Represents a mixed range of aquifer zones and conditions.
Maximum								4,600	15	-	-	2.2	0.24	0.01	0.056	

*A zone may also contribute through gravel pack.

July 1986 test pumping duration 8 hrs at 1,500 gpm.

May 1991 test pumping duration 72 hrs at 725 gpm.

Monitoring well cluster SC-18 is 39 ft from Main St well, i.e., $r = 39$ ft.

Monitoring well cluster SC-10 is 6,805 ft from Main St well.

Solution types: C=confined, UC=unconfined, L=leaky

Italics indicate value assumed for, or inferred from, previous report.

AA and A refer to Purisima Formation aquifer units; Tu refers to an older undifferentiated sandstone below the Purisima Formation (Fig. 2-2).

See Figure 3-1 for well construction and aquifer-aquitard profile.

K_V = vertical hydraulic conductivity (Neuman method); K or K_H = horizontal hydraulic conductivity

K' = aquitard hydraulic conductivity (Hantush and Hantush-Jacob methods)

K'/K ratios calculated to generate greatest range.

K'/K ratios calculated to generate greatest range.

Table 3-1

Summary of Main Street Well Aquifer-Test Analyses

Author	Pump- ing Well	Assumed		Obs. Well	Pur- isima Unit	Method	Type	Trans- missivity (<i>T</i>) (ft ² /day)	Hydraulic Conduc- tivity (<i>K</i>) (ft/day)	Solution Coefficients		<i>K_v</i> or <i>K'</i> (ft/day)	<i>K_v</i> : <i>K_H</i> or <i>K'/K</i> Ratio	Stora- tivity (<i>S</i>)	Specific Yield (<i>S_y</i>)	Comments
		Aquifer Thick- ness (<i>b</i>) (ft)	Aquitard Thick- ness (<i>b'</i>) (ft)							<i>r/B</i> or β	<i>B</i> or <i>S/S'</i>					
Fugro, 1998	Beltz 8	90	70	Beltz 8	A	Cooper-Jacob (avg)	C	9,280	103	-	-	-	-	-	-	
						Theis	C	8,920	99	-	-	-	-	-	-	
						Papadopulos-Cooper (avg)	C	7,530	84	-	-	-	-	-	-	
						Moench	L	5,220	58	-	-	-	-	-	-	
						Hantush	L	4,790	53	-	-	5.4	0.1	-	-	
						Recovery (avg)	C	7,260	81	-	-	-	-	-	-	
				Beltz 6	A	Cooper-Jacob	C	8,800	98	-	-	-	-	0.0015	-	
						Theis (avg)	C	9,690	108	-	-	-	-	0.0010	-	
						Papadopulos-Cooper (avg)	C	8,690	97	-	-	-	-	0.0047	-	
						Moench	L	6,460	72	-	-	-	-	0.0044	-	
						Hantush	L	6,690	74	-	-	0.05	0.001	0.0038	-	
						Recovery (avg)	C	8,230	91	-	-	-	-	-	-	
	Beltz 9	100	60	Beltz 9	A	Cooper-Jacob (avg)	C	6,830	68	-	-	-	-	-	-	
						Theis	C	5,570	56	-	-	-	-	-	-	
						Papadopulos-Cooper	C	6,030	60	-	-	-	-	-	-	
						Moench	L	3,880	39	-	-	-	-	-	-	
						Hantush	L	3,780	38	-	-	-	-	-	-	
						Recovery	C	5,030	50	-	-	-	-	-	-	
Johnson, 2003	Beltz 8	90	70	Beltz 8	A	Theis	C	8,900	99	-	-	-	-	-	-	
						Hantush	L	4,650	52	0.0041	0.01	0.9	0.017	-	-	
				Beltz 6	A	Theis	C	9,000	100	-	-	-	-	0.00016	-	
						Hantush-Jacob	L	8,500	94	0.0033	11,500	0.005	5E-5	0.00024	-	
						Hantush	L	5,250	58	0.05	0.1	1.0	0.017	0.00052	-	
	Beltz 9	90	60	Beltz 9	A	Neuman	UC	5,100	57	0.0025	-	0.8	0.014	0.00087	0.013	
						Theis	C	4,825	54	-	-	-	-	-	-	
						Hantush-Jacob	L	4,820	54	7.E-05	14,300	-	-	-	-	
						Hantush	L	2,370	26	1.18	0.01	-	-	-	-	
this report	Beltz 8	100	-	Beltz 8	A	<i>S_c</i> x 2000	C	6,100	61	-	-	-	-	-	-	<i>S_c</i> =22.8
			12.5			Moench	L	3,650	37	0.0047	214	1.0	0.03	0.00019	-	See Fig. 3-6
			47.5									3.8	0.10			
		100	12.5	Beltz 6	A	Moench	L	6,820	68	0.007	5,428	0.003	4E-5	0.00032	-	See Fig 3-7
			47.5									0.01	0.0001			
	Beltz 9	110	-	Beltz 9	A	<i>S_c</i> x 2000	C	5,800	53	-	-	-	-	-	-	<i>S_c</i> =21.8
			20			Moench	L	4,340	40	0.00032	769	0.15	0.004	0.014	-	See Fig 3-8
			50									0.37	0.01			
	Beltz 7	100	50	Beltz 7	A/AA	Hantush-Jacob	L	125	2.5	0.35	-	-	-	-	-	See Fig 3-9
	Average							6,100	66	n/a	n/a	1.1	0.02	0.003	0.013	
	Minimum							125	2.5	-	-	0.003	4E-5	0.0002		
	Maximum							9,700	108	-	-	5.4	0.10	0.01		

See Figure 3-_ for configuration of wells.

Solution types: C=confined, UC=unconfined, L=leaky
Beltz 6 is 38 ft from Beltz 8.

Beltz wells 8 and 9 tested at 1,200 gpm for approximately 34 hrs, in February and March 1998, respectively (Fugro, 1998).

Time-drawdown data collected from Beltz 7 during nearly 20 minutes of pumping at 260 gpm in June 2002 (City of Santa Cruz, 2002)

Italics indicate value assumed for, or inferred from, previous report

K_v = vertical hydraulic conductivity (Neuman method)*K* or *K_H* = horizontal hydraulic conductivity

K' = aquitard hydraulic conductivity (Hantush, Hantush-Jacob, and Moench methods)

Table 3-2
Summary of Beltz Well Aquifer-Test Analyses

Pumping Well/ Aquifer Unit	Test Date	Obs. Well (other than pumping well)	Test Duration (hrs)	Available Information		Pump- ing Rate (gpm)	Pumping Well Drawdown		Estimated Specific Capacity (S_c) at 24 hrs (gpm/ft)	Reported**		$Transmissivity (T)$ <i>Estimated from S_c</i> f (ft^2/day)		Screened Intervals		<i>Est. Aquifer Thick- ness</i> b_3	<i>Hydraulic Conductivity (K)</i> b_1 b_2 b_3		
							At End of Test (ft)	Extrapo- lated to 24 hrs		Trans- missivity (T) (ft^2/day)	Stora- tivity (S)			Sum b_1	Range b_2				
				Data Sheets	Data Plots														
Garnet A	#####	Opal 4	2		x	598	34	-	16.9	-	-	1,900	4,300	113	200	-	-	-	
	2			x	828	44	-	15.1	-	-	1,900	3,800							
	2			x	1,010	63	-	14.8	-	-	1,900	3,800							
	#####		8	x	x	799	52	-	15.0	4,480	-	1,900	3,800				34	19	
Rosedale AA/A	7/18- 19/83		~2		(x)	465	19	24	19.4	-	-	1,900	4,900	222	350	-	-	-	
			~2		(x)	853	36	44	19.4	-	-	1,900	4,900						
			~2		(x)	1,015	42	54	18.8	-	-	1,900	4,800			22	14		
Tannery II A	#####		2	x	x	600	44	-	-	-	-	-	-	220	235	-	-	-	
	2		x	x	800	59	-	-	-	-									
	2		x	x	1,000	81	-	-	-	-									
	2		x	x	1,400	120	-	-	-	-									
	#####		8	x	x	900	84	-	9.3	2,020	-					1,800	2,200		10
Estates A/BC	#####		2		x	700	62	-	-	-	-	-	-	415	615	-	-	-	
	2			x	1,000	90	-	-	-	-	-					-			
	2			x	1,200	112	-	-	-	-	-					-			
	#####		7		x	1,000	95	100	10.0	-	-					1,800	2,400	5.8	3.9
Madeline BC	#####		12		x	400	267	290	1.4	-	-	1,700	300	160	190	230	2.0	1.6	1.4
Ledyard BC	#####		1		x	250	110	136	1.8	-	-	1,700	400	210	215	1.9	1.8		
	1			x	350	146	195	1.8	-	-	1,700	400							
	1			x	450	188	293	1.5	-	-	1,700	300							
Bonita F/Qa	8/15- 16/83		~2		(x)	508	13	13	39.1	-	-	1,700	8,900	248	398	475	-	-	-
			~2		(x)	764	22	23	33.2	-	-	1,700	7,500						
			~2		(x)	1,050	30	33	31.8	-	-	1,700	7,200				29	18	15
San Andreas F/Qa	May-91		2		x	800	30	-	27.0	-	-	1,700	6,100	240	342	450	-	-	-
			2		x	1,000	35	-	27.8	-	-	1,700	6,300						
			2		x	1,270	44	-	27.5	-	-	1,700	6,300						
	May-91	8		x	1,040	37	-	27.8	-	-	1,700	6,300	26				18	14	
Seascape F/Qa	1987*	SC-A5	6	*	*	970	-	-	-	12,000	0.0002	-		100	240	420	120	50	29
		SC-A2		*	*												63	26	15
	1984 (see Table 3-6)		-	-	-	-	-	-	24 31	-	-	1,700	6,300						
Sells F/Qa	#####		~2		x	500	8	8	63	-	-	1,700	14,200	120	230	330	114	59	41
	~1			x	750	13	13	58	-	-	1,700	13,100	95				49	34	
	~2			x	1,000	18	20	50	-	-	1,700	11,400							
	1987*	Sc-A3 Altivo	6	*	*	560	-	-	-	66,800- 73,500	0.0008	-	-				580	310	210

Information obtained from District files, except where note
AA, A, BC, F, and Qa refer to the aquifer units defined in Figure 2-2.
(x) plot consists only of straight-line fit, no data point
Italics indicate values inferred or interpreted by this report.
* As reported in LSCE, 1987; no data or plots provided.
**Method of analysis not reported.

Estimated T (gpd/ft) = $S_c \times f$ (see Section 3.1.4 for definition of)
 T (ft²/day) = T (gpd/ft) / 7.48; $K = T/b$
Screened interval "range" is distance between uppermost and lowermost screen

Table 3-3
Summary of Soquel Creek Water District Pumping Tests

Pumping Well / Aquifer Units	Test Date	Test Duration (hrs)	Pumping Rate (gpm)	Assumed		Obs. Well	Method	Type	Transmissivity (T) (ft ² /day)	Hydraulic Conductivity (K) (ft/day)	Solution Coefficients		K _v or K' (ft/day)	K _v :K _H or K'/K Ratio	Storativity (S)	Specific Yield (S _y)	Comments
				Aquifer Thickness (b) (ft)	Aquitard Thickness (b') (ft)						r/B or β	B or S/S'					
Garnet A	#####	8	799	200	30	Garnet	Moench	L	3,350	17	0.0007	1,420	0.5	0.03	0.0002	-	See Fig. 3-10
					60								0.1	0.006			
				200	30	Opal 4 (r=30 ft)	Hantush-Jacob	L	3,390	17	0.06	500	0.4	0.02	0.0016	-	See Fig. 3-11
					60								0.8	0.05			
Tannery II A	#####	8	900	235	50	Tannery II	Hantush-Jacob	L	2,060	8.8	0.002	500	0.7	0.08	0.00055	-	See Fig. 3-12
					200								2.7	0.3			
Estates A/BC	#####	7	1,000	415 ^a	-	Estates	Theis	C	2,700	6.5	-	-	-	-	4E-5	-	See Fig. 3-13
				615 ^b				4.4									
				415 ^a	100		Hantush-Jacob	L	2,380	5.7	0.0004	2,380	0.04	0.007	0.0002	-	
				615 ^b						3.9			0.01	0.01			
Madeline BC	5/4/1984	12	400	160 ^a	-	Madeline	Theis	C	240	1.5	-	-	-	-	0.0045	-	See Fig. 3-14
				230 ^b	-			1.0									
				160 ^a	100		Hantush-Jacob	L	240	1.5	0.0010	1,000	0.02	0.02	0.0045	-	
				230 ^b	200					1.0			0.05	0.05			
				160 ^a	100		Hantush	L	240	1.5	0.0002	1	0.02	0.01	0.0045	-	
				230 ^b	200					1.0			0.03	0.03			
San Andreas F/Qa _L	May-91	8	1,040	350 ^b	-	San Andreas	Theis	C	25,000	71	-	-	-	-	8E-21	-	See Fig. 3-15
				350 ^u	20		Hantush-Jacob	L	4,700	13	0.005	200	2.4	0.2	0.001	-	Assumes thin aquitard between upper and lower Aromas.
				450 ^c	-		Neuman	UC	6,800	15	2.E-06	-	1.5	0.1	0.0002	0.06	Assumes 350-ft penetration of 450-ft aquifer.

Italics indicate unreasonable values.

^aSum of screened intervals

^bSum of screened aquifer zones.

^cWater table down to deepest screen.

Solution types: C=confined, UC=unconfined, L=leaky

AA, A, BC, F, and Qa refer to the aquifer units defined in Figure 2-2.

K_v = vertical hydraulic conductivity (Neuman method); K or K_H = horizontal hydraulic conductivity

K' = aquitard hydraulic conductivity (Hantush-Jacob and Moench methods)

Table 3-4
Summary of Re-Analyzed Pumping Tests
(other than Main Street and Beltz wells)

Well	Aquifer Unit		As Reported by Hickey (1968)*					Transmissivity (<i>T</i>) <i>Estimated from S_c</i>			Hyd. Cond. (<i>K</i>) (ft/day) <i>based on:</i>		Comments by Hickey (added comments in italics)	
	Hinkley Units	<i>this report</i>	Length of Perf. Interval <i>b₁</i> (ft)	Assumed Aquifer Thickness <i>b₂</i> (ft)	Well Yield (gpm)	Draw- down (ft)	Specific Capacity (<i>S_c</i>) (gpm/ft)							
								<i>f</i>	<i>(ft²/day)</i>	<i>b₁</i>	<i>b₂</i>			
District Service Area I														
Opal No. 3	B	A	72	200	380	32	12	-	1,900	3,000	-	42	15	
Rosedale	B	A	90	250	240	-	7	-	1,900	1,800	-	20	7.1	Lower <i>S_c</i> & <i>T</i> due to partial penetration, demonstrates low <i>K_v</i> .
					173	17	10	-	1,900	2,600	-	29	10	<i>Specific capacity suggested by provided information.</i>
Airport (Monterey)	B	A	151	255	360	36	10	-	1,800	2,400	-	16	9.4	
Malplethorpe	B	A	260	250	800	40	20	-	1,800	4,800	-	19	19	Fully penetrates unit B (i.e., unit A).
Aquifer Unit B (Hinkley)	B	A	-	230	-	-	-	-	= <i>K</i> x <i>b</i>	6,150	-		27	Assuming <i>K</i> = 200 gpd/ft ² based on Maplethorpe well.
District Service Area II														
Seacliff No. 1 (Hillcrest)	C	EF	130	150	180	30	6	-	1,700	1,400	-	10	9.1	
Seacliff No. 2	C	EF	-	150	90	33	1	3	1,700	200	600	-	1.5	<i>Provided pumping rate and drawdown suggest a different specific capacity.</i>
Seacliff No. 3	C	EF	-	150	52	74	1	-	1,700	200	-	-	1.1	Penetrates lower, siltier beds in unit C.
Seacliff No. 4	C	EF	149	150	185	54	3	-	1,700	800	-	5.2	5.2	
Aptos Creek	BC	BC/DEF	470	500	780	185	4	-	1,700	1,000	-	2.0	1.9	
Cabrillo Jr. College	BC	?	200	?	154	180	1	-	1,700	200	-	1.0	-	
Aquifer Unit C (Hinkley)	C	?	-	400	-	-	4	-	1,700	900	-	-	2.7	<i>K</i> = 20 gpd/ft ² .
District Service Areas III & IV														
Palmer	C	F	160	300	405	40	5	10	1,700	1,100	2,300	14	7.7	<i>Provided pumping rate and drawdown suggest a different specific capacity.</i>
Cliff Drive	C	F	200	350	208	46	5	-	1,700	1,000	-	5.1	2.9	
Aptos School	C	F	260	300	475	29	17	-	1,700	3,700	-	14	12	Penetrates upper, sandier beds in unit C.
Berry Farm (Country Club)	C	F/ <i>Qa_L</i>	217	300	445	18	24	-	1,700	5,600	-	26	19	Area of high <i>K</i> in unit C near Valencia Ck and Rio del Mar; Aptos well similar.
D'Anna	C	<i>Qa</i>	120	200	150	35	4	-	1,700	1,000	-	8.1	4.9	
Waugman	C	<i>Qa</i>	150	200	220	109	2	-	1,700	500	-	3.1	2.3	
La Selva No. 1	Aromas	<i>Qa</i>	10	250	225	-	6	-	1,700	1,400	-	136	5.5	<i>Specific capacity suggested by provided information.</i>
					153	26	6	-	1,700	1,300	-	134		
La Selva No. 2	Aromas	<i>Qa</i>	10	250	540	-	10	-	1,700	2,300	-	227	9.1	
					116	21	6	-	1,700	1,300	-	126	5.0	<i>Specific capacity suggested by provided information.</i>
Other														
Beltz No. 3	B	A	45	100	940	30	30	-	2,000	8,400	-	186	84	
Holm (up Soq Ck)	B	-	-	-	20	185	0.1	-	1,200	20	-	-	-	
Blake (SWN? Loc?)	B	-	-	-	610	-	20	-	1,900	5,100	-	-	-	
Rohr (Live Oak)	B	-	-	-	440	44	10	-	1,900	2,500	-	-	-	
CWD 2 (11S/1E-4Q2)	C	<i>Qa</i> /?	140	-	220	-	7	-	1,700	1,600	-	11	-	

*Added values and comments are in italics.

AA and A through F refer to Purisima aquifer units; "Qa" indicates Aromas Sands aquifer.

Estimated *T* (gpd/ft) = *S_c* × *f*; *T* (ft²/day) = *T* (gpd/ft) / 7.48; *K* = *T* / *b*.

See Section 3.1.4 for definition of *f*.

Table 3-5
Aquifer Properties Derived by and from 1968 USGS Report by Hickey

Well	Aquifer Unit	Specific Capacity (S_c)			Screened Intervals		Assumed Aquifer Thickness	Transmissivity (T) Estimated from S_c			Hydraulic Conductivity (K)									
		(Thorup, 1980)	(LSCE, 1984)								Low T			High T			Average T			
			Report Text	Hydrologic Data Appx. ^a	Sum	Range														
			b_1	b_2	b_3	b_1		b_2	b_3	b_1	b_2	b_3	b_1	b_2	b_3					
		(gpm/ft)	(ft)			f	(ft ² /day)			(ft/day)										
Opal	A	8.5	-	5.7 - 7.6	102		200	1,900	1,400 - 2,200		1,800	14		7.2	21		11	18		9.0
Opal Cliff	A	3.1	6	2 - 6	80		200	1,900	500 - 1,500		1,000	6.4		2.5	19		7.6	13		5.1
Rosedale	AA/A	-	25	19 - 32	222	350	435	1,900	4,800 - 8,100		6,500	22	14	11	37	23	19	29	19	15
Monterey	A	16.3	19	10 - 19	151		255	1,800	2,400 - 4,600		3,500	16		9.4	30		18	23		14
Maplethorpe	A	20.8	18	7 - 21	260		250	1,800	1,700 - 5,100		3,400	6.5		6.7	19		20	13		13
Tannery	A	15.6	22	8 - 11	260		260	1,800	1,900 - 5,300		3,600	7.4		7.4	20		20	13.9		13.9
Madeline	BC	4.4	3	1.8 - 2.2	160	190	230	1,700	400 - 1,000		700	2.6	2.2	1.8	6.3	5.3	4.3	4.4	3.7	3.1
Hillcrest	EF	5.7	3	2.5 - 4.5	130		150	1,700	600 - 1,300		900	4.4		3.8	10.0		8.6	7.2		6.2
Seacliff (4?)	EF	-	2	1.4 - 2.5	149		150	1,700	300 - 600		450	2.1		2.1	3.8		3.8	3.0		3.0
Aptos Creek	BC/DEF	3.7	4	3.6 - 8.8	470		500	1,700	800 - 2,000		1,400	1.7		1.6	4.3		4.0	3.0		2.8
Cliff	F	7.6	2	-	200		300	1,700	500 - 1,700		1,100	2.3		1.5	8.6		5.8	5.5		3.6
Aptos School	F	8.1	8	5.7 - 8.5	260		300	1,700	1,300 - 1,900		1,600	5.0		4.3	7.4		6.4	6.2		5.4
Country Club	F/Qa _L	18.1	20	19 - 23	169	241	300	1,700	4,100 - 5,200		4,700	24	17	14	31	22	17	28	19	16
Bonita	F/Qa _L	-	31	28 - 38	248	398	475	1,700	6,400 - 8,600		7,500	26	16	13	35	22	18	30	19	16
Seascape	F/Qa _L	-	30	24 - 31	100	240	420	1,700	5,500 - 7,000		6,300	55	23	13	70	29	17	63	26	15
Altivo	F/Qa _L	-	40	35 - 41	100	150	330	1,700	8,000 - 9,300		8,600	80	53	24	93	62	28	86	58	26
Sells	F/Qa _L	-	59	37 - 53	120	230	330	1,700	8,400 - 13,400		10,900	70	37	25	112	58	41	91	47	33

AA, A, BC, DEF, F, and Qa refer to the aquifer units defined in Figure 2-14.

^aSelected range of "adjusted" specific capacities provided in Hydrologic Data Appendix of LSCE, 1984 (highest and lowest values excluded).

Screened interval "range" is distance between uppermost and lowermost screens.

Estimated T (gpd/ft) = $S_c \times f$; T (ft²/day) = T (gpd/ft) / 7.48; $K = T/b$.

See Section 3.1.4 for definition of f .

Table 3-6

Transmissivity and Hydraulic Conductivity Estimated from Specific Capacities Reported by Thorup (1981) and LSCE (1984)

Assumed Aquifer Thickness (ft)	Well Yield (gpm)	Specific Capacity (gpm/ft)	Transmissivity (ft ² /day)	Hydraulic Conductivity (ft/day)
200 - 2,000	5 - 400	2 (max)	450	0.2 - 2

Italics indicate values inferred or interpreted by this report.

Estimated T (gpd/ft) = $S_c \times 1700$; T (ft²/day) = T (gpd/ft) / 7.48; $K = T/b$.

Table 3-7

Transmissivity and Hydraulic Conductivity Estimated from Specific Capacity North of Zayante Fault (M.J. Johnson, 1980)

Well	Reported Specific Capacity (S_c) (gpm/ft)	Aquifer Unit	Screened Intervals		Assumed Aquifer Thickness	Estimated				
			Sum	Range		Transmissivity (T)		Hydraulic Conductivity (K)		
			b_1	b_2	b_3			b_1	b_2	b_3
			(ft)			f	(ft ² /day)	(ft/day)		
Main	15.4	Tu/AA	266	420	400	1,900	3,900	15	9	10
Garnet	16.4	A	113		200	1,900	4,200	37		21
Rosedale	5.5 *	AA/A	222	350	435	1,900	1,400	6.3	4.0	3.2
Monterey	14.3	A	151		255	1,800	3,400	23		13
Maplethorpe	12.3	A	260		250	1,800	3,000	11		12
Tannery	7.2	A	260		235	1,800	1,700	6.7		7.4
Estates	12.9	A/BC	415	615	615	1,800	3,100	7.5	5.0	5.0
Madeline 2	1.7	BC	160	190	230	1,700	400	2.4	2.0	1.7
Ledyard	1.7	BC	210		215	1,700	400	1.8		1.8
T. Hopkins	2.2	DEF	255	345	385	1,700	500	2.0	1.4	1.3
Aptos Creek	7.1	BC/DEF	470		500	1,700	1,600	3.4		3.2

AA, A, BC, DEF, and F refer to the aquifer units defined in Figure 2-2.

Screened interval "range" is distance between uppermost and lowermost screens.

Estimated T (gpd/ft) = $S_c \times f$; T (ft²/day) = T (gpd/ft) / 7.48; $K = T/b$.

See Section 3.1.4 for definition of f .

Information other than column 1 original to this report.

*Low compared to pump test data summarized in Table 3-3.

Table 3-8
Transmissivity and Hydraulic Conductivity Estimated from Specific Capacities Reported by LSCE (1999)

No. Wells	Aquifer Unit	Hyd. Cond. (ft/day)
5	A	23 - 28
1	A/B/C	28
1	A-D	2.3
1	B-E	2.3
4	E	2.8 - 8.5

A through F refer to Purisima stratigraphic units (Fig. 2-2).

Table 3-9
Hydraulic Conductivities Inferred from Specific Capacities (Essaid, 1992)

Well	Assumed Aquifer Unit		Transmissivity (<i>T</i>) (ft ² /day)	Hydraulic Conductivity (<i>K</i>) (ft/day)	Storativity	Suggested Specific Capacity		Suggested Aquifer Thickness (<i>b</i>) (ft)
	M-W, 1998*	<i>this report</i>				<i>f</i>	(<i>S_c</i>) (gpm/ft)	
District Service Area I								
Main St	AA/A	AA	4,300	-	1E-6 - 5E-6	1,900	17	-
Garnet	A	<i>Tu/A</i>	4,400 - 5,800	28	1E-6 - 5E-6	1,900	17 - 23	160 - 200
Rosedale	AA/A	AA/A	3,900	28	-	1,900	15	140
Monterey	A	A	7,100	23	-	1,800	30	310
Maplethorpe	A	A	5,300 - 7,500	23	-	1,800	22 - 31	230 - 330
Tannery	A	A	2,800	23	-	1,800	12	120
District Service Area II								
Estates	A-D	<i>A/BC</i>	3,900	-	-	1,700	17	-
Madeline	B/C	<i>BC</i>	300 - 1,000	2.3	-	1,700	1 - 4	130 - 440
Hillcrest	C/D/E	<i>EF</i>	700	5.7	-	1,700	3	120
Ledyard	B	<i>BC</i>	400	-	-	1,700	2	-
Seacliff (4)	D/E/F	<i>EF</i>	300	5.7	-	1,700	1	50
T. Hopkins	B-E	<i>DEF</i>	400	-	-	1,700	2	-
Aptos Creek	B-E	<i>BC/DEF</i>	500	2.3	-	1,700	2	220
District Service Area III & IV								
Cliff	Qa	<i>F</i>	2,350	2.8	-	1,700	10	830
Country Club	Qa	<i>F/Qa_L</i>	3,800 - 4,800	-	-	1,700	17 - 21	-
Bonita	Qa	<i>F/Qa_L</i>	15,000 - 22,000	-	-	1,700	66 - 97	-
Seascape	Qa	<i>F/Qa_L</i>	16,000	-	-	1,700	70	-
San Andreas	Qa	<i>F/Qa_L</i>	27,000 - 70,000	-	-	1,700	119 - 308	-
Altivo	Qa	<i>F/Qa_L</i>	54,000	-	-	1,700	238	-
Sells	Qa	<i>F/Qa_L</i>	40,000 - 50,000	-	-	1,700	176 - 220	-
Outside District Service Area								
Beltz (?)	A	A	6,000	-	-	1,900	24	-
Beltz 4	A	A	11,000	-	-	1,900	43	-
Beltz 8	A	A	5,500	-	0.001 - 0.005	1,900	22	-
Beltz 9	A	A	6,100	-	0.001 - 0.005	1,900	24	-

*Montgomery Watson et al., 1998

Transmissivities rounded, and averaged when narrow range provided.

Italics indicate values inferred or interpreted by this report.

AA and A through F refer to Purisima aquifer units; "Qa" indicates Aromas Sands aquifer.

Estimated $S_c = T \text{ (ft}^2\text{/day)} / f \times 7.48$; $b = T/b$ (see Section 3.1.4 for definition of *f*)

Table 3-10

Aquifer Property Estimates for Individual Wells Reported in 1998 Model Report

Author	Well or Area	Aquifer Unit	Method	Transmissivity (<i>T</i>) (ft ² /day)	Storativity (<i>S</i>)	Specific Yield (<i>S_y</i>)	Assumed Aquifer Thickness (<i>b</i>) (ft)	Hydraulic Conduc- tivity (<i>K</i>) (ft/day)
Woodward- Clyde Consultants, 1983	irrigation well, Giberson Dunes (immediately south of Pajaro River mouth); observ. well at 39 ft; pumped 500 gpm for 48 hrs.	terrace deposits and possibly upper Aromas Sands	<i>S_c x 1,700</i>	7,000	-	-	103 - 200	35 - 70
			Boulton	19,400	0.00086	0.0077		97 - 190
			Cooper- Jacob	17,400	-	0.012		87 - 170
LSCE, 1987 (for PVWMA)	Northern Pajaro Valley	Aromas Sands	not reported	2,700 - 6,700	-	-	200	14 - 34
	La Selva Beach south to Sunset State Beach			2,900 - 5,600	-	-		15 - 28
	City of Watsonville well No. 17			-	0.00004	-		-
CH2M HILL, 1994	Colleg Lake area	Aromas Sands	<i>S_c x 2000</i> drillers' reports	1,800 - 5,800	-	-	150 - 300	10 - 40
	San Andreas Sand Hills			2,900 - 5,500	-	-	100 - 200	30 - 60
	Watsonville area			1,500 - 13,400	-	-	100 - 400	15 - 130
CH2M HILL, 1995	College Lake injection test well	Aromas Sands	Hantush	4,100	-	-	200	21
			Walton	3,600	-	-		18

Italics indicate values inferred or interpreted by this report.

Estimated T (gpd/ft) = $S_c \times f$; T (ft²/day) = T (gpd/ft) / 7.48; $K = T/b$.

Also see modeled values in Table 3-12.

Table 3-11
Aquifer Properties Estimated for the Pajaro Valley

Author & Area Modeled	Method	Aquifer Unit/ Model Layer	Thick- ness (<i>b</i>) (ft)	Hyd. Cond. (<i>K</i>) (ft/day)	Transmissivity (<i>T</i>) (ft ² /day)	Leakance (1/day)	Vertical Hyd. Cond. (<i>K_v</i>) (ft/day)	<i>K_v</i> : <i>K_H</i> Ratio	<i>K'</i> / <i>K</i> Ratio	Storativity (<i>S</i> = <i>S_s</i> x <i>b</i>)	Specific Storage (<i>S_s</i>) (1/ft)	Specific Yield (<i>S_y</i>)	Porosity	Comments	
Essaid, 1992 Soquel-Aptos Basin	initial guess	Purisima	2,000	8.5	17,000	1E-5	-	-	-	-	-	-	-	0.1	"Discrepancy between initial guess and calibrated <i>K</i> s because <i>S_e</i> bias to higher <i>K</i> units and effects of vertical leakage."
	model calibration	E	600	0.3	180	1E-6 - 1E-4	-	-	-	0.002	3E-6	-			
		D	100	0.3	30	1E-5 - 1E-4	-	-	-	3E-6 - 3E-5	3E-8 - 3E-7	-			
		C	120	0.3	36	1E-5 - 1E-4	-	-	-	4E-5	3E-7	-			
		B	250	0.3	75	1E-6 - 1E-4	-	-	-	8E-6 - 3E-5	3E-8 - 3E-7	-			
		AA/A	820	0.3 - 14	250 - 11,500	1E-8 - 1E-4	-	-	-	3E-5 - 3E-4	3E-8 - 3E-7	-			
	sum AA-C	1,200	-	360 - 11,600	-	-	-	-	-	-	-	-	-		
	sum AA-D	1,300	-	390 - 11,600											
	sum B-E	1,070	-	320											
sum AA-E	1,900	-	570 - 11,800												
M-W et al., 1998 Soquel-Aptos Basin	model calibration	Qal	varies	5 - 100	varies	0.5	-	-	-	-	-	0.1	-	Values of <i>S</i> < 1E-6 not realistic; perhaps are <i>S_s</i> values (?).	
		Qa _U		5 - 40		0.14	-	-	-	-	-	0.06			
		Qa _L		5 - 30		0.2 - 2	-	-	-	-	-	0.06			
		D/E/F		0.5 - 50		0.1 - 1	-	-	-	1E-6	-	?			
		C		0.5 - 35		0.1 - 1	-	-	-	5E-7 - 2E-6	-				
		B		0.05 - 0.4		0.02 - 0.05	-	-	-	5E-7 - 2E-6	-				
		AA/A		0.02 - 0.4		0.25 - 0.6	-	-	-	2E-7 - 5E-7	-				
		Handel et al., 1985 Soq-Ap basin		initial guess		Purisima aquifer	varies	86	varies	-	-	-	-		-
model calibration	0.86														
Johnson, 2003 Live Oak-Soquel	conceptual model	above B	varies	2	varies	-	1	0.5	-	5E-4	-	0.06	0.08		
		B	80	5	400	0.02	1	0.2	0.2						
		A-B aquitard	40	1	40	0.02	1	1	-						
		A	100	10 - 50	1,000 - 5,000	0.02	2	0.2 - 0.04	0.1 - 0.02						
		AA-A aquitard	40	1	40	0.01	1	1	-						
		AA	130	10	1,300	0.004	1	0.1	0.75						
		below AA	400	7.5	3,000	-	1	0.13	-						
		sum (B and below)	790	7 - 12	5,800 - 9,800	-	-	-	-						
Todd Engineers, 2002; Aptos to La Selva Beach	conceptual model	Qa (and F?)	267	106	28,350	-	-	-	-	-	-	-	-	Aromas aquifer thickness representative of northern Pajaro Valley.	
RMC, 2000 Pajaro Valley	model calibration	Qa/Qt	200	0.52 - 300	100 - 60,000	-	2E-7 - 0.5	-	-	1E-6 - 1E-4	-	0.04 - 0.14	0.15		
Bond and Bredehoeft, 1987 Pajaro Valley	conceptual model	Qal	-	-	6,500	-	-	-	-	0.002	-	-	-		
		Qa	300	43	13,000	-	-	-	-	-	-	-	-		
Johnson, M. and others, 1988 Pajaro Valley	model calibration	layer 1	120+	26 - 35	varies	9E-4 - 0.9	-	-	-	-	-	0.05 - 0.06		Upper and lower Aromas in Soquel-Aptos study area.	
		layer 2	-	-	13,000	0.0015	-	-	-	-	0.001	-			0.05
		layer 3	-	-	7,800	-	-	-	-	-	1E-4	-			-

Italics indicate values inferred or interpreted by this report from information provided in the original studies.

AA and A through F = Purisima units; "Qa" = Aromas Sands aquifer; "Qal" and "Qt" = alluvial and terrace deposits, respectively.

Table 3-12
Aquifer Properties Used in Previous Soquel-Aptos and Pajaro Valley Groundwater Models

Hydro-geologic Unit	Thickness* (ft)		Transmissivity (T) (ft ² /day)	Hydraulic Conductivity (K) (ft/day)	Vertical Hydraulic Cond. (K _v) (ft/day)	Storativity (S)	Specific Yield (S _y)
	Avg	Range					
Qa _U	-	< 100	-	3 - 40	0.05 - 2	-	0.04 - 0.14
Qa _L	175	130 - 220	1,200 - 10,000	6 - 50	0.05 - 2	1E-5 - 0.007	
Tp inland**		200 - 2,000	200 - 500	0.2 - 2	0.001 - 0.1		0.01 - 0.10
F	200	100 - 300	400 - 1,200	2 - 6	0.005 - 0.5		
DEF	330	300 - 360	600 - 1,600	2 - 6	0.005 - 0.5		
D (aquitard)	80	60 - 100	1 - 75	0.005 - 1	0.001 - 0.1		
BC	200	150 - 230	200 - 450	1 - 3	0.005 - 0.1		
B (aquitard)	150	130 - 185	1 - 150	0.005 - 1	0.001 - 0.1		
A	250	200 - 280	2,000 - 3,500	7 - 18	0.05 - 2		
A (lower)	100	-	3,600 - 6,800	30 - 65	0.1 - 2		
AA	220	160 - 300	300 - 2,400	1 - 10	0.001 - 0.1		
Tp? (aquitard)	100	< 200	1 - 200	0.005 - 1	0.001 - 0.1		
Tu	150	< 300	100 - 3,000	1 - 20	0.01 - 0.5		
Purisima Total	1,500	1,100 - 2,000	3,500 - 13,000	3 - 7	-	-	-

*All unit thicknesses range to zero where the unit pinches out due to erosion at the land surface.

**e.g., north of Zayante fault.

Table 3-13

Estimated Aquifer Properties for Soquel-Aptos Hydrogeologic Units

Calendar Year	Reported Annual Totals*			Sum of Monthly Totals by Well**					Sum of Months minus Reported Annual		
	Purisima Wells	Aromas Wells	Total	Service Area				Total	I & II	III & IV	Total
				I	II	III	IV				
1966	1,468	613	2,081								
1967	1,530	702	2,232								
1968	1,729	610	2,339								
1969	1,811	689	2,501								
1970	1,894	768	2,662								
1971	1,961	840	2,801								
1972	2,319	958	3,277								
1973	2,501	926	3,427								
1974	2,256	953	3,208								
1975	2,432	1,004	3,436								
1976	2,541	1,054	3,595								
1977	2,374	1,050	3,424								
1978	2,749	1,239	3,988								
1979	2,868	1,297	4,165								
1980	2,994	1,345	4,339								
1981	3,021	1,238	4,259								
1982	3,107	1,311	4,418								
1983	3,288	1,592	4,880								
1984	3,218	1,701	4,919	2,209	1,008	1,518	242	4,977	0	59	58
1985	3,139	1,872	5,011	2,163	976	1,626	253	5,018	0	7	7
1986	3,245	1,892	5,137	2,257	988	1,408	276	4,929	0	-208	-208
1987	3,230	1,712	4,942	2,230	1,200	1,615	304	5,349	200	207	407
1988	3,170	2,007	5,177	2,182	993	1,708	300	5,183	5	1	6
1989	3,155	1,917	5,072	2,068	1,089	1,611	307	5,075	2	1	3
1990	3,268	1,738	5,006	2,030	1,239	1,441	298	5,008	2	1	3
1991	3,147	1,614	4,762	1,900	1,249	1,330	282	4,761	1	-2	-1
1992	3,329	1,756	5,085	1,978	1,353	1,448	309	5,087	2	1	3
1993	3,317	1,731	5,048	2,005	1,314	1,407	321	5,047	2	-2	0
1994	3,438	1,768	5,206	2,023	1,413	1,422	345	5,203	-2	-1	-3
1995	3,488	1,784	5,272	2,136	1,350	1,440	343	5,269	-2	-1	-3
1996	3,591	1,831	5,421	2,228	1,361	1,482	347	5,418	-2	-1	-3
1997	3,783	2,105	5,887	2,396	1,384	1,721	383	5,884	-2	-1	-3
1998	3,353	1,766	5,119	2,278	1,073	1,421	344	5,116	-2	-1	-3
1999	3,362	2,070	5,432	2,433	927	1,746	360	5,465	-2	36	34
2000	3,446	2,028	5,474	2,497	939	1,661	366	5,463	-10	-1	-11
2001	3,366	2,119	5,485	2,251	1,063	1,887	230	5,431	-52	-2	-54
2002	3,421	2,196	5,617	2,316	1,104	2,079	114	5,613	-1	-3	-4
2003	3,439	2,107	5,546								
N	38	38	38	19	19	19	19	19			
Avg	2,888	1,471	4,359	2,188	1,159	1,577	301	5,226			
% of Total	66%	34%	100%	42%	22%	30%	6%	100%			
Min	1,468	610	2,081	1,900	927	1,330	114	4,761			
Max	3,783	2,196	5,887	2,497	1,413	2,079	383	5,884			

*LSCE, September 2003.

**SCWD data base and records for Hillcrest well.

Table 4-1a
SCWD Annual Groundwater Production, 1966-2002
(ac-ft/yr)

CY	Service Area I							Service Area II							CY
	Opal #1 (A)	Garnet (A)	Main St (Tu/AA)	Rosedale (AA/A)	Monterey (A)	Maple- thorpe (A)	Tannery (A)	Estates (A/BC)	Madeline (BC)	Ledyard (BC)	Hillcrest (DEF)	Seacliff 4 (F)	T. Hopkins (DEF)	Aptos Ck (BC/DEF)	
1984	285	-	-	685	464	270	506	-	187	-	127	210	-	484	1984
1985	195	-	-	1,008	418	184	357	-	280	-	267	20	-	410	1985
1986	186	-	-	960	385	196	529	17	187	175	221	-	-	388	1986
1987	202	-	-	1,020	329	179	499	618	58	276	77	-	-	172	1987
1988	146	-	240	953	146	193	503	586	36	286	-	-	-	84	1988
1989	50	-	464	781	171	146	456	813	49	149	-	-	-	78	1989
1990	42	-	549	777	167	142	353	741	50	98	-	-	138	212	1990
1991	42	-	575	615	161	157	349	352	60	226	-	-	281	331	1991
1992	4	-	663	511	138	181	480	721	62	238	-	-	95	237	1992
1993	117	-	624	490	114	195	466	661	27	187	-	-	178	259	1993
1994	175	-	701	380	126	183	457	727	81	54	-	-	232	318	1994
1995	195	-	684	593	125	48	490	600	139	98	-	-	208	305	1995
1996	88	120	720	620	123	99	459	576	135	76	-	-	241	333	1996
1997	-	281	885	607	131	22	470	576	114	35	-	-	285	374	1997
1998	-	400	745	438	140	228	327	510	65	68	-	-	200	230	1998
1999	-	413	820	446	194	235	325	457	107	0	-	-	173	189	1999
2000	-	389	1,066	426	262	9	344	462	92	0	-	-	222	164	2000
2001	-	427	942	548	233	-	102	499	108	12	-	-	221	223	2001
2002	-	371	1,010	602	176	-	157	436	102	34	-	-	219	314	2002
2003															2003
Avg	133	343	712	656	157	211	402	550	102	118	173	115	207	269	Avg

CY	Service Area III & IV								Service Areas					CY
	Cliff (F)	Aptos Jr. H.S. (F/Qa)	Country Club (F/Qa)	Bonita (F/Qa)	San Andreas (F/Qa)	Seascape (F/Qa)	Sells (F/Qa)	Altivo (F/Qa)	I	II	III	IV	Total	
1984	62	211	225	612	-	407	61	181	2,209	1,008	1,518	242	4,977	1984
1985	26	181	140	948	-	332	135	118	2,163	976	1,626	253	5,018	1985
1986	-	120	169	568	-	551	133	143	2,257	988	1,408	276	4,929	1986
1987	-	-	143	772	-	700	141	163	2,230	1,200	1,615	304	5,349	1987
1988	-	-	273	788	-	647	147	153	2,182	993	1,708	300	5,183	1988
1989	-	-	220	681	-	710	149	158	2,068	1,089	1,611	307	5,075	1989
1990	-	-	156	668	-	617	143	155	2,030	1,239	1,441	298	5,008	1990
1991	-	-	141	662	-	528	136	146	1,900	1,249	1,330	282	4,761	1991
1992	-	-	151	527	240	530	150	159	1,978	1,353	1,448	309	5,087	1992
1993	-	-	139	467	504	298	156	165	2,005	1,314	1,407	321	5,047	1993
1994	-	-	187	513	386	336	177	168	2,023	1,413	1,422	345	5,203	1994
1995	-	-	265	487	386	303	165	178	2,136	1,350	1,440	343	5,269	1995
1996	-	-	315	437	370	361	175	173	2,228	1,361	1,482	347	5,418	1996
1997	-	-	263	453	599	406	161	222	2,396	1,384	1,721	383	5,884	1997
1998	-	-	221	445	452	302	153	191	2,278	1,073	1,421	344	5,116	1998
1999	-	-	213	554	336	643	130	230	2,433	927	1,746	360	5,465	1999
2000	-	-	225	431	524	481	162	204	2,497	939	1,661	366	5,463	2000
2001	-	-	231	448	565	643	87	143	2,251	1,063	1,887	230	5,431	2001
2002	-	-	195	479	678	727	44	70	2,316	1,104	2,079	114	5,613	2002
2003														2003
Avg	44	171	204	576	458	501	137	164	2,188	1,159	1,577	301	5,226	Avg

Table 4-1b
SCWD Annual Groundwater Production (by well and service area), 1984-2002 (ac-ft/yr)

Calendar Year	City of Santa Cruz Beltz Wells	Central Water District Cox and Rob Roy Wells
1962	583	-
1963	598	-
1964	752	-
1965	782	142
1966	813	140
1967	141	140
1968	170	140
1969	134	140
1970	133	140
1971	171	140
1972	817	140
1973	660	140
1974	420	132
1975	378	-
1976	763	-
1977	148	-
1978	262	-
1979	26	-
1980	105	-
1981	462	-
1982	235	-
1983	309	-
1984	446	-
1985	536	-
1986	103	418
1987	1,196	438
1988	1,319	435
1989	916	416
1990	698	440
1991	549	415
1992	811	475
1993	416	481
1994	519	469
1995	276	485
1996	168	521
1997	245	622
1998	306	531
1999	284	540
2000	574	538
2001	526	578
2002	441	595
2003		
N	41	27
Avg	468	363
Min	26	132
Max	1,319	622

1962-1974 from Muir, 1980

1972-2002 Beltz from City of Santa Cruz Water Department (same as Muir for 1972-74)

1986-2002 from Central Water District

**Table 4-2
City of Santa Cruz and
Central Water District
Annual Groundwater
Production (ac-ft/yr)**

Quarter	Service Area I							Service Area II						
	Opal 1 (A)	Garnet (A)	Main Street (Tu/AA)	Rose- dale (AA/A)	Maple- thorpe (A)	Tannery (A)	Monterey (A)	Estates (A/BC)	Madeline (BC)	Hill- crest* (EF)	Seacliff 4** (EF)	Ledyard (BC)	Aptos Creek (BC/DEF)	T. Hopkins (DEF)
Aut-83	28.70				43.60	98.57	69.80		33.41	8.57				82.77
Win-84	42.55				82.65	179.15	108.64		9.12	7.40	39.90			153.76
Spr-84	93.12			135.64	82.87	220.87	126.67		2.16	10.52	56.70			148.64
Sum-84	90.90			296.89	76.72	105.94	122.19		101.31	64.79	67.20			120.21
Aut-84	58.24			252.29	27.33	0.03	106.33		74.73	44.54	46.20			61.31
Win-85	54.60			224.12	30.78	19.25	102.55		71.83	38.47	3.80			42.20
Spr-85	49.22			285.28	46.24	88.97	111.85		83.28	54.67	5.40			123.94
Sum-85	51.90			293.42	68.92	143.99	109.53		76.16	102.86	6.40			146.71
Aut-85	39.17			205.38	38.16	105.11	94.30		48.30	70.71	4.40			97.11
Win-86	38.92			188.53	35.78	94.21	74.21		20.86	61.07		43.08		68.05
Spr-86	51.38			280.56	54.01	144.95	111.60	14.79	64.24	86.78		54.81		101.72
Sum-86	57.76			279.86	56.95	155.11	113.14	2.24	67.20	43.24		28.05		126.64
Aut-86	38.17			211.47	49.29	135.02	86.14		34.36	29.73		48.67		92.02
Win-87	24.30			183.32	37.01	106.83	89.88	10.82	21.01	25.67		57.72		79.87
Spr-87	60.58			286.67	47.46	150.74	110.24	221.66	13.93	36.48		64.74		36.33
Sum-87	91.04			304.03	54.15	162.82	92.09	245.44	11.53	14.73		78.04		32.35
Aut-87	26.33			246.14	40.82	78.72	36.80	140.15	11.05			75.49		23.20
Win-88	22.28		169.50	182.94	25.49	66.54	24.70	97.57	0.70			66.41		22.84
Spr-88	37.61		38.01	279.66	57.98	125.94	46.66	156.62	7.58			69.66		25.32
Sum-88	67.03		20.47	303.95	64.94	164.23	33.82	203.62	15.78			82.34		15.98
Aut-88	18.89		12.07	186.89	44.71	146.72	40.65	128.30	12.01			67.73		20.05
Win-89	11.03		10.94	177.11	38.74	119.00	42.06	114.30	10.58			53.50		14.14
Spr-89	16.13		113.08	219.14	42.96	137.88	43.15	197.13	10.61			63.47		17.01
Sum-89	12.67		208.84	199.39	36.82	120.86	44.86	256.52	13.69			32.47		22.52
Aut-89	10.21		130.89	185.76	27.44	78.73	40.47	244.79	13.86					23.90
Win-90	8.68		141.35	189.76	10.52	31.61	38.65	202.90	11.19			23.94		14.80
Spr-90	11.18		109.51	200.02	46.94	130.67	43.82	224.50	12.17			59.22		20.12
Sum-90	11.97		157.04	195.91	59.80	136.29	43.95	259.06	12.80			15.20		52.98
Aut-90	9.90		141.31	191.47	24.29	54.80	40.54	54.19	13.66					124.51
Win-91	8.99		108.64	140.48	26.66	59.73	39.03	25.03	9.00			46.29		91.94
Spr-91	12.34		155.39	156.16	44.72	96.77	40.70	70.22	9.30			61.60		103.70
Sum-91	10.59		169.38	179.42	54.78	121.75	40.30	143.48	20.26			61.54		81.15
Aut-91	10.40		141.82	139.03	30.81	71.11	40.94	112.82	21.18			56.10		53.80
Win-92	3.98		130.67	90.32	34.56	81.44	38.12	111.20	15.14			47.00		36.26
Spr-92			155.70	159.47	52.09	152.59	38.54	182.92	16.00			55.47		65.49
Sum-92			195.37	158.68	58.87	153.95	36.04	252.98	14.52			76.21		82.38
Aut-92			181.52	102.23	35.97	92.49	25.07	174.18	15.96			59.41		52.58
Win-93			165.77	82.11	35.05	84.09	16.44	132.03	13.54			30.81		59.17
Spr-93	13.24		193.31	141.11	53.76	130.01	3.31	178.02				48.19		68.53
Sum-93	61.90		87.09	185.21	69.77	167.32	60.46	209.24	3.50			64.57		70.46
Aut-93	41.78		177.39	81.17	36.20	84.81	34.08	142.11	10.36			43.87		61.30
Win-94	40.56		143.14	64.38	37.17	86.93	31.44	157.16	3.43					69.18
Spr-94	41.33		196.88	61.82	62.63	152.58	33.09	209.06	12.49			11.19		83.13
Sum-94	45.45		214.10	146.40	53.88	139.59	31.63	223.95	30.33			19.38		100.06
Aut-94	47.73		147.30	107.46	29.22	78.12	30.26	136.97	34.99			23.70		65.91
Win-95	45.70		136.88	92.18	9.00	70.78	30.90	115.82	31.68			24.27		58.61
Spr-95	43.28		158.98	146.68	21.26	119.76	31.27	152.91	35.76			24.29		77.85
Sum-95	54.27		224.61	206.70	11.93	183.69	33.78	187.19	37.69			24.97		96.74
Aut-95	52.08		163.50	147.82	5.70	115.83	29.31	144.45	33.68			24.79		71.66
Win-96	49.29		151.49	131.65	3.26	58.46	31.56	99.57	33.38			24.82		61.05
Spr-96	29.73		202.97	176.73	9.35	152.58	31.44	171.22	32.64			25.18		82.57
Sum-96	8.79	59.52	220.54	190.02	50.27	148.48	30.69	178.72	36.36			25.35		100.89
Aut-96		60.06	144.75	121.88	35.83	98.98	29.40	126.58	33.08			0.22		88.11
Win-97		76.76	140.33	105.41	20.97	73.57	33.65	127.18	29.09					68.31
Spr-97		85.84	236.13	191.39		151.77	34.79	184.63	32.98			1.08		100.32
Sum-97		41.80	315.71	193.68	1.35	156.28	48.42	136.03	34.47			11.69		116.97
Aut-97		76.35	192.55	117.00	0.01	88.79	13.92	128.49	17.01			22.15		88.25
Win-98		94.77	162.48	82.83	19.38	59.53		117.68	10.97			11.16		66.75
Spr-98		95.11	167.98	92.73	51.13	67.23	44.66	154.41	5.89			13.63		74.22
Sum-98		106.16	248.86	165.39	110.56	128.22	49.07	103.46	23.68			36.64		72.18
Aut-98		104.05	165.76	97.06	46.58	71.75	46.55	134.05	24.64			6.27		17.30
Win-99		99.89	156.86	79.96	42.68	57.23	46.73	78.51	26.63			0.11		17.79
Spr-99		107.16	205.71	127.12	71.29	92.90	51.87	122.05	27.06			0.04		60.05
Sum-99		107.46	262.54	140.16	76.94	107.51	48.79	158.92	26.99					66.34
Aut-99		98.32	194.43	98.72	44.48	67.78	46.79	97.44	26.53					45.14
Win-00		98.51	223.50	83.21	8.81	72.93	54.38	55.79	27.28					23.78
Spr-00		85.59	319.47	72.64		135.19	81.14	73.76	30.93					79.52
Sum-00		104.46	315.57	173.25		51.03	77.99	186.76	27.38					60.44
Aut-00		100.60	207.93	97.20		84.42	48.89	145.96	5.97					
Win-01		91.67	187.60	96.74		72.97	50.63	89.02	26.45					
Spr-01		116.63	293.07	157.36	0.07	28.97	69.23	139.38	28.70			8.28		51.24
Sum-01		114.69	298.53	159.79	0.00	0.03	79.01	142.95	26.93					96.36
Aut-01		103.87	162.33	133.71		0.01	33.99	127.87	26.29			3.71		75.09
Win-02		99.35	191.86	116.16			27.51	17.84	27.60			10.34		86.52
Spr-02		103.21	309.94	169.85		5.89	60.43	140.64	26.55			10.77		79.75
Sum-02		97.75	278.94	158.09		85.29	47.63	196.04	25.66			13.02		102.30
Aut-02		70.38	228.84	158.09		66.22	40.23	81.16	22.19			0.04		45.00
Win-03		91.43	128.26	147.96		16.56	38.96	92.01	26.78					55.87
Spr-03		88.23	116.73	157.54		196.58	35.84	118.41	26.06					69.67
Sum-03		167.58	121.67	182.58		228.18	35.18	182.65	27.16					101.89
N	48	29	63	78	67	79	79	69	79	16	8	56	78	51
Avg	37	95	175	166	40	103	53	141	26	44	29	36	69	56
Min	4	42	11	62	0	0	3	2	1	7	4	0	14	16
Max	93	168	319	304	111	228	127	259	101	103	67	82	154	122

*Estimated from fiscal-year totals.

**Estimated from difference between total and sum of wells.

Table 4-3a
Quarterly Groundwater Production, 1983-1993 (ac-ft)
Service Area I and II Wells

Quarter	Service Area III						S.A. IV		Service Area Total			
	Aptos Jr. H.S. (F/Qa)	Country Club (F/Qa)	Sea- scape (F/Qa)	Bonita (F/Qa)	San Andreas (F/Qa)	Cliff (F)	Sells (F/Qa)	Altivo (F/Qa)	I	II	III	IV
Aut-83	20.48	48.45	89.22			8.51		25.43	240.66	124.75	166.65	25.43
Win-84	45.75	79.65	131.73			14.85		41.44	413.00	210.18	271.99	41.44
Spr-84	72.70	81.50	129.78	144.24		25.11		70.47	659.18	218.02	453.33	70.47
Sum-84	60.41	44.14	110.51	267.80		12.86	36.54	49.24	692.64	353.51	495.72	85.78
Aut-84	32.62	20.20	35.19	200.08		8.85	24.57	19.60	444.23	226.78	296.94	44.16
Win-85	35.19	19.55	68.66	180.26		7.48	22.43	23.55	431.30	156.30	311.14	45.98
Spr-85	59.22	34.08	70.86	272.45		6.87	41.85	31.55	581.56	267.28	443.48	73.40
Sum-85	52.40	52.40	108.21	302.16		8.85	43.14	37.23	667.76	332.13	524.03	80.37
Aut-85	33.96	33.96	83.89	193.25		2.71	27.61	25.20	482.11	220.52	347.76	52.81
Win-86	26.93	37.03	86.68	86.68			24.07	22.78	431.66	193.06	237.33	46.85
Spr-86	45.64	49.63	108.30	108.30			39.07	43.11	642.51	322.35	311.87	82.18
Sum-86	47.08	59.19	180.01	199.72			40.85	44.35	662.82	267.38	485.99	85.20
Aut-86		23.10	176.19	173.64			28.88	33.19	520.09	204.78	372.93	62.07
Win-87		19.99	160.63	110.51			24.98	25.34	441.34	195.10	291.13	50.31
Spr-87		23.74	186.03	214.37			40.29	50.63	655.69	373.14	424.14	90.92
Sum-87		29.56	267.59	273.60			47.42	51.90	704.13	382.08	570.75	99.32
Aut-87		69.63	85.66	173.79			28.79	34.83	428.81	249.90	329.08	63.61
Win-88		63.43	92.69	219.06			30.12	31.99	491.45	187.51	375.18	62.11
Spr-88		93.89	204.41	164.18			39.25	44.94	585.86	259.19	462.48	84.19
Sum-88		67.80	216.72	223.67			48.55	45.48	654.44	317.72	508.18	94.03
Aut-88		48.31	133.41	180.75			29.10	30.66	449.92	228.09	362.48	59.76
Win-89		40.28	120.79	153.38			25.64	26.85	398.90	192.53	314.44	52.49
Spr-89		63.62	215.72	180.23			41.89	46.45	572.33	288.22	459.57	88.34
Sum-89		68.24	245.93	190.34			47.87	49.87	623.44	325.21	504.51	97.74
Aut-89		48.03	127.44	157.05			34.06	34.51	473.50	282.56	332.52	68.56
Win-90		36.09	91.43	147.68			25.60	28.41	420.56	252.82	275.20	54.00
Spr-90		47.07	176.95	164.52			42.93	39.92	542.14	316.01	388.54	82.85
Sum-90		36.21	209.03	198.83			41.89	50.14	604.97	355.89	444.07	92.03
Aut-90		36.65	139.89	156.63			32.28	36.79	462.32	314.73	333.16	69.07
Win-91		37.14	86.71	132.32			24.01	27.49	383.52	257.17	256.17	51.50
Spr-91		33.60	153.74	172.03			35.68	39.22	506.06	330.53	359.36	74.90
Sum-91		35.09	169.64	203.72			44.12	45.84	576.22	372.67	408.45	89.95
Aut-91		34.92	118.00	153.54			32.07	33.32	434.12	288.28	306.45	65.39
Win-92		32.94	69.01	151.08			24.57	26.44	379.09	251.77	253.02	51.01
Spr-92		38.64	182.79	174.51	29.78		43.79	47.20	558.39	372.79	425.71	90.99
Sum-92		45.07	183.88	110.02	114.53		48.57	52.11	602.92	426.08	453.50	100.68
Aut-92		34.72	93.86	91.25	95.58		32.86	33.68	437.28	302.13	315.42	66.54
Win-93		31.24	50.21	83.68	80.45		22.00	25.70	383.45	253.73	245.58	47.69
Spr-93		36.68	154.02	98.90	91.89		43.45	43.75	534.75	347.82	381.48	87.20
Sum-93		38.03	56.90	168.73	198.11		48.19	62.78	631.76	404.48	461.76	110.97
Aut-93		32.60	36.67	115.47	133.23		42.48	33.14	455.42	307.59	317.97	75.63
Win-94		31.55	42.43	108.33	96.93		41.58	22.23	403.63	280.92	279.24	63.81
Spr-94		33.28	84.97	139.44	133.26		45.36	51.56	548.33	380.73	390.94	96.92
Sum-94		55.90	149.81	175.18	68.88		54.61	59.82	631.05	444.63	449.77	114.43
Aut-94		66.19	59.16	90.09	86.68		35.17	34.40	440.08	306.58	302.13	69.57
Win-95		63.26	29.71	86.82	73.28		30.21	28.33	385.44	269.78	253.07	58.54
Spr-95		66.18	71.50	121.37	99.74		45.40	39.74	521.21	342.75	358.79	85.15
Sum-95		65.89	141.60	155.71	114.37		50.56	69.11	714.99	411.52	477.57	119.67
Aut-95		69.62	59.86	122.73	98.33		38.66	40.89	514.24	326.03	350.54	79.55
Win-96		77.82	28.92	85.01	65.88		31.26	26.30	425.71	264.39	257.63	57.56
Spr-96		77.47	116.79	115.95	107.22		49.38	49.81	602.81	374.75	417.41	99.20
Sum-96		80.47	159.43	127.30	114.17		56.82	60.49	708.32	411.58	481.38	117.30
Aut-96		78.78	55.78	108.73	82.40		37.19	36.14	490.89	310.01	325.69	73.34
Win-97		64.42	40.29	111.62	102.24		24.71	39.60	450.69	281.17	318.57	64.31
Spr-97		67.28	143.06	97.40	196.68		38.36	75.59	699.92	399.49	504.42	113.95
Sum-97		66.91	168.64	134.69	180.88		58.94	64.88	757.25	383.90	551.12	123.83
Aut-97		64.47	53.85	109.52	118.78		39.41	41.47	488.62	319.22	346.62	80.88
Win-98		60.83	8.20	88.71	93.68		29.02	29.52	418.99	252.43	251.42	58.54
Spr-98		59.94	76.58	115.73	101.37		41.19	40.33	518.86	305.60	353.62	81.51
Sum-98		65.27	121.92	135.28	150.76		56.66	71.77	808.25	274.13	473.23	128.43
Aut-98		34.81	95.71	105.67	106.21		26.35	49.46	531.75	240.94	342.40	75.81
Win-99		39.54	98.95	82.18	93.74		0.06	59.61	483.35	141.16	314.42	59.67
Spr-99		58.47	194.14	108.84	125.40		34.39	65.70	656.06	262.70	486.84	100.09
Sum-99		59.50	256.11	192.70	22.96		57.67	62.88	743.38	313.78	531.27	120.55
Aut-99		55.66	93.56	170.20	93.56		37.84	41.85	550.53	208.88	412.98	79.69
Win-00		55.87	21.91	117.72	98.28		30.93	36.94	541.34	128.40	293.78	67.87
Spr-00		54.91	164.99	101.37	160.76		40.54	66.14	694.03	261.66	482.03	106.68
Sum-00		57.28	228.30	118.78	133.13		54.94	63.27	722.30	346.89	537.49	118.21
Aut-00		57.36	66.03	92.80	131.46		35.52	38.03	539.04	202.38	347.65	73.55
Win-01		46.80	33.34	119.70	94.55		33.76	32.26	499.62	147.7589	294.38	66.02
Spr-01		54.36	172.55	150.45	130.06		43.59	60.18	665.33	280.98	507.42	103.77
Sum-01		70.61	263.08	136.42	175.09		1.77	33.18	652.05	344.21	645.21	34.95
Aut-01		59.15	173.68	41.37	165.57		7.58	17.44	433.92	290.28	439.77	25.02
Win-02		30.75	109.70	100.09	108.80		10.85	12.87	434.88	205.27	349.33	23.72
Spr-02		55.57	242.47	123.95	180.39		9.12	13.12	649.32	311.39	602.38	22.25
Sum-02		55.87	262.29	126.01	231.46		14.21	27.04	667.71	404.53	675.63	41.26
Aut-02		53.26	112.23	129.02	157.62		9.44	17.05	563.77	183.30	452.13	26.49
Win-03		51.36		129.94	192.02		4.81	11.47	423.17	217.94	373.32	16.27
Spr-03		59.38	75.85	147.36	258.98		11.07	12.81	594.92	268.59	541.56	23.87
Sum-03		71.01	269.48	158.24	202.49		9.40	38.72	735.19	391.16	701.21	48.12
N	12	80	79	78	46	9	77	80	80	80	80	80
Avg	44	51	126	146	124	11	34	40	545	288	397	73
Min	20	20	8	41	23	3	0	11	241	125	167	16
Max	73	94	269	302	259	25	59	76	808	445	701	128

Table 4-3b
Quarterly Groundwater Production, 1983-1993 (ac-ft)
Service Area III and IV Wells and Service Area Totals

Water Year	Autumn Oct-Dec	Winter Jan-Mar	Spring Apr-Jun	Summer Jul-Sep	Total	% of Avg
1965	18.54	8.47	3.52	0.11	30.64	99%
1966	11.59	7.28	1.04	0.57	20.48	66%
1967	13.09	16.74	10.17	0.00	40.00	130%
1968	5.37	14.39	1.15	0.55	21.46	70%
1969	13.08	28.80	2.99	0.07	44.94	146%
1970	9.86	19.53	0.79	0.00	30.18	98%
1971	18.97	5.91	1.98	0.38	27.24	88%
1972	11.70	3.92	2.09	1.37	19.08	62%
1973	17.33	25.84	0.09	0.41	43.67	142%
1974	18.54	15.34	5.19	2.89	41.96	136%
1975	6.92	13.65	2.73	0.99	24.29	79%
1976	4.44	6.14	2.31	2.48	15.37	50%
1977	6.89	5.54	1.02	1.36	14.81	48%
1978	8.07	23.51	5.39	0.62	37.59	122%
1979	5.56	21.44	1.95	0.20	29.15	94%
1980	12.76	20.68	2.99	0.71	37.14	120%
1981	2.78	18.18	0.61	0.17	21.74	70%
1982	12.67	27.85	6.37	1.25	48.14	156%
1983	11.96	34.06	5.68	2.23	53.93	175%
1984	17.79	4.67	1.44	0.11	24.01	78%
1985	17.04	11.59	0.76	0.29	29.68	96%
1986	10.51	27.37	1.37	1.74	40.99	133%
1987	1.78	13.23	0.84	0.00	15.85	51%
1988	11.15	5.23	2.35	0.00	18.73	61%
1989	12.54	9.88	0.84	0.94	24.20	78%
1990	3.36	8.62	4.57	0.21	16.76	54%
1991	2.79	16.33	1.12	0.12	20.36	66%
1992	8.02	18.64	0.83	0.02	27.51	89%
1993	8.51	25.31	2.87	0.00	36.69	119%
1994	7.34	11.51	3.80	0.06	22.71	74%
1995	8.48	26.52	8.01	0.00	43.01	139%
1996	6.73	20.75	4.01	0.00	31.49	102%
1997	23.51	11.67	0.96	0.46	36.60	119%
1998	13.73	38.89	7.12	0.08	59.82	194%
1999	7.92	22.18	3.35	0.20	33.65	109%
2000	4.47	28.33	3.06	0.53	36.39	118%
2001	7.16	16.21	1.86	0.22	25.45	82%
2002	18.05	9.53	1.16	0.05	28.79	93%
2003	19.48	5.14	4.26	0.00	28.88	94%
2004						
N	39	39	39	39	39	39
Avg	10.78	16.64	2.89	0.55	30.86	100%
Min	1.78	3.92	0.09	0.00	14.81	48%
Max	23.51	38.89	10.17	2.89	59.82	194%

Station's monthly record extends back to 1867.

Table 4-4
Quarterly and Water-Year Precipitation
Santa Cruz NOAA Station, 1965-2003
(inches/year)

Well		Date	Cal- cium (Ca)	Magne- sium (Mg)	So- dium (Na)	Potas- sium (K)	Car- bonate (CO ₃)	Bicar- bonate (HCO ₃)	Sul- fate (SO ₄)	Chlor- ide (Cl)	Nitrate (NO ₃)	Iron (Fe)	TDS	Na:Cl Molar Ratio
			(mg/L)											
Main Street (AA,Tu)	N	21	12	12	12	12	11	11	11	17	10	11	11	11
	Min	4/25/1988	31	13	5.4	4.0		150	31	13		ND	270	0.64
	Max	10/7/2003	57	21	52	6.8		190	80	28		0.46	370	4.17
	Avg	4/14/1997	42	16	34	5.3	ND	172	49	20	ND	0.29	330	2.49
Opal 1 (A)	N	49	29	29	23	21	20	21	22	46	21	49	24	22
	Min	#####	64	11	27	4.5		140	106	39	ND	ND	480	0.43
	Max	1/27/1998	260	132	39	6.4		226	200	100	2.5	100	660	0.95
	Avg	1/22/1971	128	38	30	5.5	ND	178	146	67	0.66	3.80	566	0.65
Opal 2 (A)	N	6	1	1	1	1	1	1	1	5	1	6	2	1
	Min	4/28/1950								29		ND	250	0.48
	Max	5/25/1993								86		270	598	0.48
	Avg	#####	104	22	27	5.7	ND	180	146	51	ND	7.02	424	0.48
Opal 3 (A)	N	34	18	18	12	11	9	10	12	31	12	34	13	12
	Min	7/6/1951	82	13	27	4.4	ND	145	83	27	ND	0.05	250	0.51
	Max	4/17/1986	258	98	43	6.4	7.2	235	177	87	3.6	6.20	612	1.14
	Avg	6/2/1968	138	37	32	5.5	7.2	187	139	53	0.87	1.09	526	0.78
Opal 4 (A)	N	5	5	5	5	5	5	5	5	5	5	5	5	5
	Min	9/3/1981	91	15	28	5.4		150	128	63	ND	0.47	490	0.46
	Max	4/18/1989	117	22	37	6.1		195	162	94	0.5	1.20	571	0.69
	Avg	6/12/1984	104	18	30	5.7	ND	178	145	78	0.50	0.68	545	0.61
Garnet (A)	N	11	10	10	10	10	8	8	8	8	7	10	8	8
	Min	9/15/1998	94	19	30	5.5		140	160	69		ND	540	0.58
	Max	#####	120	26	35	6.8		160	180	88		1.50	670	0.73
	Avg	5/11/2002	112	24	33	6.0	ND	156	170	81	ND	1.39	599	0.63
Monterey (A)	N	61	19	19	13	12	11	11	12	54	11	30	12	12
	Min	4/4/1945	69	17	55	6.9		220	87	54		ND	420	1.39
	Max	10/7/2003	221	156	75	9.4		370	120	71		10.10	710	1.99
	Avg	5/21/1980	115	42	63	7.9	ND	246	95	62	ND	0.71	542	1.64
Rosedale (AA,A)	N	52	13	13	13	13	10	11	11	46	9	21	12	11
	Min	3/21/1949	52	14	48	5.1		210	69	35	ND	ND	320	1.51
	Max	10/7/2003	100	24	55	8.0		230	120	68	1.5	3.90	550	2.21
	Avg	5/2/1976	71	18	52	6.5	ND	221	87	50	1.5	0.90	474	1.92
Maplethrope (A)	N	36	29	29	24	22	23	23	25	32	24	36	25	23
	Min	4/21/1965	70	15	7.1	6.5		200	96	64	ND	ND	471	0.16
	Max	6/13/2001	226	97	94	64.0		308	230	150	2.3	2.60	850	1.63
	Avg	3/23/1979	104	33	67	10.3	ND	269	121	76	0.50	0.38	585	1.37
Tannery (A)	N	39	14	14	14	13	11	11	12	35	11	14	12	12
	Min	9/12/1973	20	17	57	6.4		230	55	39		ND	421	1.01
	Max	10/7/2003	100	31	100	9.4		260	160	110		0.88	990	3.95
	Avg	5/14/1990	82	22	69	8.0	ND	246	105	65	ND	0.31	604	1.80
Service Area I (except Main St) (AA,A)	N	293	138	138	115	108	98	101	108	262	101	205	113	106
	Min	#####	20	11	7	4.4	ND	140	55	27	ND	0.05	250	0.16
	Max	#####	260	156	100	64.0	7.2	370	230	150	3.6	100	990	3.95
	Avg	12/7/1979	106	30	45	7	7	207	128	65	1	1.81	541	1.10

Table 4-5a
Production Well Water Quality, SCWD Wells

Well		Date	Cal- cium (Ca)	Magne- sium (Mg)	So- dium (Na)	Potas- sium (K)	Car- bonate (CO ₃)	Bicar- bonate (HCO ₃)	Sul- fate (SO ₄)	Chlor- ide (Cl)	Nitrate (NO ₃)	Iron (Fe)	TDS	Na:Cl Molar Ratio
			(mg/L)											
Estates (A,BC)	N	26	15	15	15	15	13	13	13	23	11	13	13	12
	Min	5/31/1985	52	13	70	6.4		230	61	41		ND	440	2.34
	Max	10/7/2003	72	17	86	8.5		290	78	63		0.30	550	2.90
	Avg	#####	64	16	78	7.6	ND	258	67	48	ND	0.20	493	2.60
Madeline (BC)	N	33	13	13	13	12	11	11	13	31	12	12	12	13
	Min	9/12/1973	32	19	64	3.0	ND	240	43	21	ND	ND	280	1.61
	Max	8/5/2003	82	73	100	5.3	60	270	91	71	1	0.47	587	4.82
	Avg	3/6/1990	40	27	81	3.7	60	253	58	36		0.25	422	3.17
Ledyard (BC)	N	16	7	7	7	7	6	6	7	15	7	6	6	14
	Min	5/24/1985	16	15	55	3.0		210	45	28		ND	270	1.77
	Max	8/7/2002	30	40	110	4.1		260	72	87		0.23	460	12.00
	Avg	9/13/1993	25	23	89	3.5	ND	226	64	44	ND	0.13	382	4.07
T-Hopkins (DEF)	N	19	12	12	12	12	11	11	12	13	10	13	12	10
	Min	4/16/1991	30	25	39	4.8		200	49	38		ND	290	1.07
	Max	10/7/2003	49	48	67	7.0		260	70	59		0.95	460	2.60
	Avg	1/10/1999	40	37	51	6.0	ND	226	61	47	ND	0.22	408	1.64
Aptos Creek (BC,DEF)	N	49	42	42	36	33	33	33	35	44	34	45	35	32
	Min	1/21/1965	22	19	24	2.0	ND	170	34	29	ND	ND	310	0.88
	Max	10/7/2003	98	221	69	9.7	7.2	318	110	50	7	2.44	550	3.13
	Avg	1/4/1986	47	52	51	5.8	6.1	264	81	41	1.63	0.37	437	1.90
Service Area II (A,BC,DEF)	N	143	89	89	83	79	74	74	80	126	74	89	78	81
	Min	1/21/1965	16	13	24	2.0	0	170	34	21	0	0.00	270	0.88
	Max	10/7/2003	98	221	110	9.7	60	318	110	87	7	2.44	587	12.00
	Avg	#####	43	31	70	5.3	33	245	66	43	1.63	0.23	428	2.68
Hillcrest (DEF)	N	30	22	22	16	14	14	14	15	28	15	29	15	15
	Min	10/2/1951	25	19	21	2.8	ND	204	50	22	ND	ND	376	0.43
	Max	4/9/1987	178	160	89	5.8	32	304	98	135	2.5	2,000	590	4.16
	Avg	5/11/1973	83	68	44	3.9		258	77	63	0.71	77	465	1.19
Seacliff 2 (DEF)	N	3	0	0	1	0	1	1	0	3	0	3	1	1
	Min	6/6/1951								34		0.17		
	Max	7/10/1967								45		0.25		
	Avg	#####			35		ND	352		40		0.21	364	1.35
Seacliff 3 (DEF)	N	2	0	0	1	0	1	1	1	2	0	2	0	1
	Min	10/2/1951								44		ND		
	Max	#####			40		ND	320	44	48		0.85		1.40
Seacliff 4 (DEF)	N	32	22	22	15	14	14	14	15	31	15	32	15	15
	Min	3/18/1955	14	8.3	29	2.0	ND	151	28	25	ND	ND	276	0.73
	Max	4/9/1987	80	117	125	5.9	23	283	73	64	29	2.40	462	7.71
	Avg	9/13/1972	36	55	43	5.1	14.5	194	46	52	3.03	0.34	342	1.60
State Park (DEF)	N	3	0	0	0	0	0	0	0	3	0	3	0	0
	Min	5/15/1959								44		0.21		
	Max	10/6/1961								113		8.20		
	Avg	3/3/1960								68		3.40		
Old Seacliff Wells (DEF)	N	70	44	44	33	28	30	30	31	67	30	69	31	32
	Min	6/6/1951	14	8	21	2.0	0	151	28	22	0	0.17	276	0.43
	Max	4/9/1987	178	160	125	5.9	32	304	98	135	29	2,000	590	7.71
	Avg	1/30/1964	59	62	41	4.5	14.5	281	56	54	1.87	16	390	1.38

Table 4-5a

Production Well Water Quality, SCWD Wells

Well	Date	Cal- cium (Ca)	Magne- sium (Mg)	So- dium (Na)	Potas- sium (K)	Car- bonate (CO ₃)	Bicar- bonate (HCO ₃)	Sul- fate (SO ₄)	Chlor- ide (Cl)	Nitrate (NO ₃)	Iron (Fe)	TDS	Na:Cl Molar Ratio
		(mg/L)											
Country Club (Qa/F)	N	34	25	25	19	18	16	18	20	32	18	31	19
	Min	10/2/1956	27	21	20	1.9		135	28	21	1	ND	220
	Max	8/6/2003	119	136	44	6.0		212	37	33	24	0.65	342
	Avg	12/4/1984	46	48	25	2.8	ND	173	34	28	13	0.15	303
Bonita (Qa/F)	N	20	18	18	18	17	17	18	18	16	17	17	18
	Min	3/28/1995	26	19	19	2.3		150	25	18	4.9	ND	230
	Max	8/6/2003	37	33	24	3.4		190	34	26	14	0.07	310
	Avg	10/7/1999	32	26	22	2.9	ND	166	30	22	8.21	0.05	284
San Andreas (Qa/F)	N	22	20	20	20	19	19	20	20	18	19	19	19
	Min	5/20/1993	24	18	15	2.3		150	8.6	16	1.8	ND	190
	Max	8/6/2003	34	28	24	3.8		170	42	22	12	0.05	340
	Avg	3/9/1999	30	23	20	3.0	ND	160	23	19	5.56	0.04	257
Seascape (Qa/F)	N	45	22	22	17	16	15	15	17	44	15	22	16
	Min	9/21/1964	24	17	16	2.4		120	14	13	2.5	ND	170
	Max	8/6/2003	94	82	19	3.0		140	18	26	8	0.19	251
	Avg	#####	38	33	17	2.8	ND	133	16	20	6.33	0.06	228
Altivo (Qa/F)	N	20	18	18	18	17	17	18	18	16	17	17	18
	Min	3/28/1995	16	10	8.9	1.8		80	4	11	3.8	ND	95
	Max	8/6/2003	31	25	21	3.0		150	22	22	9.7	0.02	250
	Avg	10/6/1999	21	13	12	2.1	ND	98	8	15	6.05	0.02	173
Sells (Qa/F)	N	20	18	18	18	17	17	18	18	16	17	17	18
	Min	3/28/1995	18	11	10	1.3		86	5	12	6.9	ND	100
	Max	8/6/2003	33	26	24	2.9		150	23	29	27	0.03	280
	Avg	10/7/1999	24	16	16	1.9	ND	113	11	19	15	0.03	207
Service Areas III & IV (Qa/F)	N	161	121	110	108	101	103	111	150	99	123	105	109
	Min	10/2/1956	16	10	8.9	1.3	0	80	4	11	1	ND	95
	Max	8/6/2003	119	136	44	6	0	212	42	33	27	0.65	342
	Avg	1/16/1995	32	27	19	2.57	ND	141	20	21	8.89	0.06	242.1

Max and min dates correspond to the period of record and not dates of other max and min values.

Averages ignore "non-detects" (ND); service area averages are averages of averages.

TDS = total dissolved solids

Table 4-5a
Production Well Water Quality, SCWD Wells

Well		Date	Cal- cium (Ca)	Magne- sium (Mg)	So- dium (Na)	Potas- sium (K)	Alka- linity	Sul- fate (SO ₄)	Chlor- ide (Cl)	Nitrate (NO ₃)	Iron (Fe)	Mang- anese (Mn)	Conduc- tivity (uS/cm)
			(mg/L)										
Beltz 2 (A)	N	21	9	9		16	16	12	12	13	12	13	16
	Min	7/24/1974	48	14		7.4	110	40	65	0.04	0.4	0.02	480
	Max	4/21/1999	96	31		8.1	138	59	180	0.5	1.6	0.34	1,230
	Avg	6/25/1990	65	19		7.6	125	49	116	0.2	1.0	0.23	840
Beltz 4 (A)	N	11	6	6		7	7	7	7	5	6	6	7
	Min	5/23/1980	76	16		6.75	120	2	54	0.09	3.5	0.44	740
	Max	#####	117	22		7.5	158	68	60	1.1	14	0.72	925
	Avg	#####	91	18		7.2	141	41	57	0.4	6.6	0.54	816
Beltz 6 (A)	N	25	11	11		15	14	14	14	14	15	15	15
	Min	7/7/1970	38	10		7.2	94	27	39	0.004	0.8	0.10	360
	Max	8/30/1995	56	31		7.6	139	39	50	1.0	2.8	0.36	690
	Avg	11/6/1984	50	14		7.4	112	32	44	0.2	1.3	0.17	508
Beltz 7 (AA,A)	N	124	13	13	1	19	35	97	97	102	96	15	116
	Min	5/17/1974	49	10		7.2	134	ND	11	0.001	0.2	0.22	225
	Max	#####	167	83		7.8	178	239	67	3.2	87	1.0	1,240
	Avg	5/27/2000	128	28	20	7.6	157	69	37	0.9	5.9	0.75	638
Beltz 8 (A)	N	39	1	1		1	22	5	5	11	11	7	26
	Min	9/29/1999					88	37	43	0.1	1.5	0.11	410
	Max	#####					152	120	46	0.5	1.7	0.18	1,180
	Avg	1/11/2002	60	18		7.4	122	78	45	0.3	1.6	0.15	672
Beltz 9 (A)	N	31	1	1		1	20	5	5	11	5	1	24
	Min	2/16/2000					84	77	35	0.2	ND		450
	Max	#####					170	97	67	0.7	0.4		975
	Avg	8/4/2002	43	14		7.8	131	87	51	0.5	0.4	0.04	675
Beltz Wells (AA,A)	N	251	41	41	1	59	114	140	140	156	145	57	204
	Min	7/7/1970	38	10		6.8	84	2	11	0.001	0.2	0.017	225
	Max	#####	167	83		8.1	178	239	180	3.2	87	1.0	1,240
	Avg	#####	73	19	20	7.5	131	59	58	0.4	2.8	0.3	692

Max and min dates correspond to the period of record and not dates of other max and min values.

Averages ignore "non-detects" (ND)

TDS = total dissolved solids

Table 4-5b
Production Well Water Quality
Beltz Wells

Well		Date	Cal- cium (Ca)	Magne- sium (Mg)	So- dium (Na)	Potas- sium (K)	Car- bonate (CO ₃)	Bicar- bonate (HCO ₃)	Sul- fate (SO ₄)	Chlor- ide (Cl)	Nitrate (NO ₃)	Iron (Fe)	TDS	Na:Cl Molar Ratio
			(mg/L)											
SC-1A	N	8	8	8	8	8	8	8	8	8	8	8	8	8
	Min	1/5/1996	40	8.3	19	3.4		105	41	21		0.43	190	0.71
	Max	1/6/2003	91	19	26	4.6		140	180	54		4.3	630	1.76
	Avg	7/11/1999	58	11	23	3.8	ND	121	77	32	ND	1.48	318	1.19
SC-3A	N	8	8	8	8	8	8	8	8	8	8	8	8	8
	Min	1/9/1996	41	7	39	5.1		200	98	25		0.22	360	1.72
	Max	1/22/2003	49	8.9	105	6.1		220	110	42		1.5	510	5.49
	Avg	7/14/1999	46	8	86	5.5	ND	209	102	36	ND	0.74	433	3.74
SC-3B	N	8	8	8	8	8	8	8	8	8	8	8	8	8
	Min	1/9/1996	16	1.2	72	3		110	56	30		0.66	255	2.52
	Max	1/22/2003	48	10	94	4.3		180	73	44		20	380	4.68
	Avg	7/14/1999	25	4	82	3.7	ND	129	63	35	ND	7.23	303	3.71
SC-3C	N	7	7	7	7	7	7	7	7	7	7	7	7	7
	Min	1/9/1996	70	18	34	3.1		170	94	40		1.15	375	0.78
	Max	1/22/2003	100	26	80	4.8		260	110	75		3.8	540	2.47
	Avg	4/28/1999	90	21	43	3.9	ND	209	99	54	ND	2.38	450	1.26
SC-5A	N	6	6	6	6	6	6	6	6	6	6	6	6	6
	Min	1/9/1996	59	13	38	5.3		235	81	30		0.91	460	1.20
	Max	1/16/2002	73	18	91	6.5		270	130	67		13	570	4.68
	Avg	7/14/1998	65	15	79	5.9	ND	250	104	52	ND	3.46	518	2.54
SC-5B	N	6	6	6	6	6	6	6	6	6	6	6	6	5
	Min	1/11/1996	43	13	140	3.2		145	190	120	2.5	0.17	640	1.35
	Max	1/16/2002	64	30	170	4.9		180	240	160	2.5	4.9	780	2.18
	Avg	7/15/1998	50	18	160	3.8	ND	162	215	132	2.5	1.37	708	1.87
SC-5C	N	2	2	2	2	2	2	2	2	2	2	2	2	2
	Min	1/13/1999	77	42	66	6.9		190	200	130		4	700	0.78
	Max	1/14/2002	100	47	91	7.5		200	220	130		5	720	1.08
	Avg	7/15/2000	89	45	79	7.2	ND	195	210	130	ND	4.50	710	0.93
SC-8A	N	7	7	7	7	7	7	7	7	7	7	7	7	7
	Min	1/14/1997	1.7		100	1.7	0	45	78	11		0.06	310	12.12
	Max	1/14/2003	1.7		120	3.5	105	150	88	14		0.24	340	16.12
	Avg	1/15/2000	2	ND	112	2.1	73	77	82	12	ND	0.14	331	14.50
SC-8B	N	7	7	7	7	7	7	7	7	7	7	7	7	7
	Min	1/15/1997	5	0	61	2.3	0	160	61	12		0.07	310	3.76
	Max	1/15/2003	22	17	165	6.7	33	185	135	32		0.18	460	19.92
	Avg	#####	12	10	116	3.6	12	167	98	20	ND	0.11	389	11.58
SC-8C	N	7	7	7	7	7	7	7	7	7	7	7	7	7
	Min	1/16/1997	3.5		96	2.3	0	177	42	12		0.05	320	7.79
	Max	1/15/2003	7		160	4.3	26	200	135	22		0.28	440	20.56
	Avg	1/17/2000	5	ND	119	2.6	11	187	58	18	ND	0.18	351	10.76
SC-8D	N	7	7	7	7	7	7	7	7	7	7	7	7	7
	Min	1/15/1997	3.2		100	2.3	0	182	43	17		0.06	320	8.06
	Max	1/15/2003	6		125	4.1	20	200	50	22		0.11	360	9.74
	Avg	1/16/2000	5	ND	114	2.6	8	191	46	19	ND	0.08	337	9.10
SC-8E	N	7	7	7	7	7	7	7	7	7	7	7	7	7
	Min	1/16/1997	14	14	57	4.3		155	59	25		0.06	310	3.33
	Max	1/15/2003	21	18	70	6		160	68	31		0.09	340	4.13
	Avg	1/15/2000	17	17	66	4.8	ND	159	63	28	ND	0.08	325	3.64
SC-8F	N	7	7	7	7	7	7	7	7	7	7	7	7	7
	Min	1/16/1997	86	115	205	11.5		5	100	620	3.5	0.76	1,400	0.34
	Max	1/16/2003	820	390	950	61		150	310	3,650	3.5	5.2	8,500	0.51
	Avg	1/17/2000	417	284	637	39.8	ND	61	229	2,490	3.5	2.08	5,040	0.41

Well		Date	Cal- cium (Ca)	Magne- sium (Mg)	So- dium (Na)	Potas- sium (K)	Car- bonate (CO ₃)	Bicar- bonate (HCO ₃)	Sul- fate (SO ₄)	Chlor- ide (Cl)	Nitrate (NO ₃)	Iron (Fe)	TDS	Na:Cl Molar Ratio
			(mg/L)											
SC-9A	N	8	7	7	7	7	8	8	8	8	7	8	8	7
	Min	1/10/1996	5.8	1.3	77	2.3		160	4.4	16		ND	315	2.16
	Max	1/21/2003	23	11	130	5.1		250	110	55		31	470	12.05
	Avg	7/18/1999	15	8	105	3.7	ND	195	52	34	ND	10.63	368	6.52
SC-9B	N	7	6	6	6	6	7	7	7	7	6	7	7	6
	Min	1/11/1996	4.7		130	1.2	0	150	140	19		ND	375	9.39
	Max	1/21/2003	7		160	2.6	20	180	160	23		0.91	510	12.99
	Avg	#####	6	ND	148	2.2	3.33	169	150	21	ND	0.31	454	11.1
SC-9C	N	7	6	6	6	6	7	7	7	7	6	7	7	6
	Min	1/11/1996	11	1.7	100	4.6	0	190	53	30		ND	340	4.79
	Max	1/21/2003	19	4.6	125	6.3	15	330	60	37		3.5	420	6.17
	Avg	#####	16	3	117	5.4	4.17	233	57	34	ND	1.51	394	5.40
SC-9D	N	7	6	6	6	6	7	7	7	7	6	7	7	6
	Min	1/10/1996	26	12	65	2.7		205	27	43		ND	325	1.88
	Max	1/21/2003	31	18	87	5		220	44	58		4.7	420	3.05
	Avg	#####	30	15	78	4.1	ND	211	33	51	ND	1.51	378	2.48
SC-9E	N	7	6	6	6	6	7	7	7	7	6	7	7	6
	Min	1/10/1996	65	35	26	3.3	0	218	125	36	3.5	ND	460	0.89
	Max	1/21/2003	86	49	59	3.8	10	280	140	86	3.5	6.8	580	1.29
	Avg	#####	75	42	34	3.5	1.67	243	131	47	3.5	2.86	522	1.12
SC-10A	N	8	8	8	8	8	8	8	8	8	7	8	8	8
	Min	1/5/1996	91	19	31	4.8		220	125	34		2.1	425	0.92
	Max	1/6/2003	110	28	38	5.9		260	175	53		7.6	600	1.59
	Avg	7/12/1999	100	25	35	5.4	ND	232	141	46	ND	3.86	517	1.21
SC-10AA	N	8	7	7	7	7	8	8	8	8	7	8	8	7
	Min	1/11/1996	35	12	11	3.6		150	9.5	7.7		ND	165	1.41
	Max	1/8/2003	43	14	13	4		160	14	12		4.6	260	2.40
	Avg	7/12/1999	38	14	12	3.8	ND	155	11	10	ND	1.97	216	1.80
SC-A1A	N	6	5	5	5	5	6	6	6	6	4	6	6	5
	Min	12/5/1995	18	19	26	2.6	0	137	15	25		ND	210	1.24
	Max	#####	23	22	29	8.8	20	145	20	36		0.69	260	1.73
	Avg	6/8/1999	20	20	28	7.1	5	142	17	29	ND	0.30	237	1.53
SC-A1B	N	6	5	5	5	5	6	6	6	6	4	6	6	5
	Min	12/5/1995	2.7	20	19	2.9		150	11	22		ND	230	1.06
	Max	#####	32	28	22	3.4		175	18	32		0.07	270	1.41
	Avg	6/8/1999	24	24	20	3.1	ND	165	15	26	ND	0.04	251	1.23
SC-A1C	N	6	5	5	5	5	6	6	6	6	5	6	6	5
	Min	12/5/1995	34	20	22	2.6		160	39	25	3	ND	250	0.97
	Max	#####	37	29	24	2.9		180	45	35	4.5	0.94	330	1.42
	Avg	6/9/1999	36	26	23	2.7	ND	167	42	30	3.62	0.59	303	1.20
SC-A1D	N	6	5	5	5	5	6	6	6	6	5	6	6	5
	Min	12/5/1995	31	19	21	2.6		150	35	17	3.1	ND	260	1.12
	Max	#####	39	28	25	2.8		180	44	30	3.1	0.5	320	2.00
	Avg	6/10/1999	35	23	22	2.7	ND	168	40	24	3.1	0.21	299	1.50
SC-A2A	N	8	7	7	7	7	8	8	8	8	7	8	8	7
	Min	12/5/1995	1,700	1,275	1,930	28		120	120	9,120	1.3	ND	18,000	0.27
	Max	12/9/2002	2,070	1,800	2,500	115		140	1,600	13,000	40	0.23	23,400	0.34
	Avg	6/5/1999	1,880	1,550	2,120	54	ND	129	1,210	10,800	26	0.17	21,000	0.31

Well		Date	Cal- cium (Ca)	Magne- sium (Mg)	So- dium (Na)	Potas- sium (K)	Car- bonate (CO ₃)	Bicar- bonate (HCO ₃)	Sul- fate (SO ₄)	Chlor- ide (Cl)	Nitrate (NO ₃)	Iron (Fe)	TDS	Na:Cl Molar Ratio
			(mg/L)											
SC-A2B	N	7	6	6	6	6	7	7	7	7	6	7	7	6
	Min	12/5/1995	55	28	39	3.8		49	100	94		ND	460	0.29
	Max	12/9/2002	70	63	52	4.9		140	120	280		2.3	750	0.69
	Avg	8/26/1999	65	48	47	4.3	ND	123	109	161	ND	0.50	604	0.46
SC-A2C	N	8	7	7	7	7	8	8	8	8	7	8	8	7
	Min	12/5/1995	44	36	45	2		90	71	150	16	ND	530	0.46
	Max	12/9/2002	74	46	75	2.7		130	89	245	27	0.26	700	0.66
	Avg	6/5/1999	58	40	65	2.3	ND	108	77	199	19.571	0.11	624	0.51
SC-A3A	N	8	7	7	7	7	8	8	8	8	7	8	8	7
	Min	12/5/1995	760	690	7,760	37		150	2,010	15,800	52	ND	35,000	0.75
	Max	#####	1,240	1,100	10,200	3,160		170	3,100	22,000	58	0.85	37,800	0.83
	Avg	4/21/1999	988	942	8,750	500	ND	158	2530	17,800	55	0.61	36,200	0.78
SC-A3B	N	7	6	6	6	6	7	7	7	7	6	7	7	6
	Min	12/5/1995	515	215	190	9.1		110	190	1,800	1.5	ND	3,700	0.15
	Max	#####	900	475	605	33		130	390	2,750	2.7	0.9	8,800	0.34
	Avg	5/10/1999	664	348	357	17	ND	116	255	2,330	2.1	0.43	5,140	0.22
SC-A3C	N	9	7	7	7	7	8	8	8	8	8	9	8	7
	Min	12/5/1995	37	8.7	28	2		99	18	23	24	ND	270	1.06
	Max	#####	50	23	44	3.1		170	24	64	56	0.66	380	2.61
	Avg	8/26/1999	44	15	37	2.3	ND	136	21	39	43	0.16	334	1.64
SC-A4A	N	9	9	9	9	9	9	9	9	9	8	9	9	9
	Min	#####	1,300	780	995	20		115	680	6,530		0.1	12,000	0.21
	Max	#####	1,750	1,130	1,650	190		140	1,000	8,740		0.19	16,400	0.33
	Avg	10/9/1999	1,600	953	1,175	42	ND	124	811	7,540	ND	0.15	14,200	0.24
SC-A4B	N	8	8	8	8	8	8	8	8	8	7	8	8	8
	Min	#####	39	20	16	3.1		170	39	14		0.13	260	0.90
	Max	#####	47	23	18	4.4		185	50	29		0.32	320	1.98
	Avg	10/2/1999	44	22	17	3.6	ND	176	42	18	ND	0.25	289	1.53
SC-A4C	N	8	8	8	8	8	8	8	8	8	8	8	8	8
	Min	#####	34	21	19	2.2		180	37	9.4	1.2		270	1.81
	Max	#####	46	26	21	3.4		190	46	17	1.2		300	3.45
	Avg	4/1/2000	41	23	21	2.8	ND	185	39	13	1.2	ND	289	2.50
SC-A4D	N	8	6	6	6	6	6	6	6	6	8	8	6	6
	Min	12/4/1998	24	14	26	1.4		83	10	16	49	ND	220	1.01
	Max	#####	33	19	30	2		180	46	46	74	0.068	290	2.60
	Avg	2/19/2001	28	16	28	1.6	ND	106	27	33	58	0.04	257	1.48
SC-A5A	N	8	8	8	8	8	8	8	8	8	7	8	8	8
	Min	#####	875	815	400	34		92	485	4,150		0.07	9,000	0.12
	Max	#####	1,100	1,100	490	48		120	610	5,600		0.14	11,200	0.17
	Avg	5/2/1999	971	981	441	39.5	ND	103	553	5,060	ND	0.10	10,129	0.14
SC-A5B	N	8	8	8	8	8	8	8	8	8	7	8	8	8
	Min	#####	26	24	37	2.6		140	115	16		0.15	340	1.58
	Max	#####	36	37	40	3.2		150	130	39		0.54	460	3.86
	Avg	6/13/1999	31	31	39	2.8	ND	144	122	24	ND	0.32	381	2.82
SC-A5C	N	8	8	8	8	8	8	8	8	8	7	8	8	8
	Min	#####	22	16	15	2.1		135	15	11	1.3		220	1.22
	Max	#####	27	26	17	2.7		160	29	21	1.7		555	2.10
	Avg	6/12/1999	26	21	16	2.4	ND	143	21	18	1.47	ND	274	1.44
SC-A5D	N	8	7	7	7	7	7	7	7	7	7	8	7	7
	Min	#####	19	11	16	1.8		88	2.7	26	6.8	ND	175	0.73
	Max	#####	26	13	18	2.1		120	7.1	36	15	0.4	200	1.07
	Avg	1/8/2000	22	12	17	2.0	ND	93	5	31	10	0.14	185	0.87

Averages ignore "non-detects" (ND); TDS = total dissolved solids.

Table 4-6

SCWD Monitoring Well Water Quality

Aquifer		Date	Cal- cium (Ca)	Magne- sium (Mg)	So- dium (Na)	Potas- sium (K)	Car- bonate (CO ₃)	Bicar- bonate (HCO ₃)	Sul- fate (SO ₄)	Chlor- ide (Cl)	Nitrate (NO ₃)	Iron (Fe)	TDS	Na:Cl Molar Ratio
			(mg/L)											
Tp-F (SC-8F)	N	7	7	7	7	7	7	7	7	7	7	7	7	7
	Min	1/16/1997	86	115	205	11.5		5	100	620	3.5	0.76	1,400	0.34
	Max	1/16/2003	820	390	950	61		150	310	3,650	3.5	5.2	8,500	0.51
	Avg	1/17/2000	417	284	637	40	ND	61	229	2,490	3.5	2.1	5,040	0.41
Tp-E	N	14	13	13	13	13	14	14	14	14	13	14	14	13
	Min	1/10/1996	14	14	26	3.3	0	155	59	25		ND	310	0.89
	Max	1/21/2003	86	49	70	6	10	280	140	86		6.8	580	4.1
	Avg	#####	46	30	50	4.2	1.7	201	97	38	ND	1.5	424	2.38
		Wells:		SC-8E	SC-9E									
Tp-D	N	14	13	13	13	13	14	14	14	14	13	14	14	13
	Min	1/10/1996	3.2	12	65	2.3	0	182	27	17		ND	320	1.88
	Max	1/21/2003	31	18	125	5	20	220	50	58		4.7	420	9.7
	Avg	#####	17	15	96	3.4	8.0	201	39	35	ND	0.79	358	5.79
		Wells:		SC-8D	SC-9D									
Tp-C	N	23	22	22	22	22	23	23	23	23	22	23	23	22
	Min	1/9/1996	3.5	1.7	34	2.3	0	170	42	12		ND	320	0.78
	Max	1/22/2003	100	47	160	7.5	26	330	220	130		5	720	20.6
	Avg	#####	50	23	89	4.8	7.5	206	106	59	ND	2.1	476	4.59
		Wells:		SC-3C	SC-5C	SC-8C	SC-9C							
Tp-B	N	28	27	27	27	27	28	28	28	28	27	28	28	26
	Min	1/9/1996	4.7	0	61	1.2	0	110	56	12	2.5	ND	255	1.35
	Max	1/22/2003	64	30	170	6.7	33	185	240	160	2.5	20	780	19.9
	Avg	6/20/1999	23	10	126	3.3	7.8	157	131	52	2.5	2.3	463	7.06
		Wells:		SC-3B	SC-5B	SC-8B	SC-9B							
Tp-A	N	45	44	44	44	44	45	45	45	45	43	45	45	44
	Min	1/5/1996	1.7	1.3	19	1.7	0	45	4.4	11		0	190	0.71
	Max	1/22/2003	110	28	130	6.5	105	270	180	67		31	630	16.1
	Avg	6/14/1999	47	13	73	4.4	73	181	93	35	ND	3.4	414	4.95
		Wells:		SC-1A	SC-3A	SC-5A	SC-8A	SC-9A	SC-10A					
AA (SC-10AA)	N	8	7	7	7	7	8	8	8	8	7	8	8	7
	Min	1/11/1996	35	12	11	3.6		150	9.5	7.7		ND	165	1.41
	Max	1/8/2003	43	14	13	4		160	14	12		4.6	260	2.40
	Avg	7/12/1999	38	14	12	3.8	ND	155	11	10	ND	2.0	216	1.80
Qa/F (not intruded)	N	65	56	56	56	56	61	61	61	61	56	65	61	56
	Min	12/5/1995	2.7	8.7	15	1.4	0	83	2.7	9.4	1.2	ND	175	0.73
	Max	#####	50	29	44	8.8	20	190	46	64	74	0.94	555	3.4
	Avg	#####	31	20	24	3.0	5.0	145	25	27	17	0.21	270	1.49
		Wells:		SC-A1A	SC-A1B	SC-A1C	SC-A1D	SC-A3C	SC-A4C	SC-A4D	SC-A5C	SC-A5D		
Qa/F (transi- tional)	N	31	29	29	29	29	31	31	31	31	27	31	31	29
	Min	12/5/1995	26	20	16	2		49	39	14	16	ND	260	0.29
	Max	#####	74	63	75	4.9		185	130	280	27	2.3	750	3.9
	Avg	7/27/1999	49	35	42	3.2	ND	138	88	101	20	0.30	475	1.33
		Wells:		SC-A2B	SC-A2C	SC-A4B	SC-A5B							
Qa/F (intruded)	N	40	37	37	37	37	40	40	40	40	35	40	40	37
	Min	12/5/1995	515	215	190	9.1		92	120	1,800	1.3	ND	3,700	0.12
	Max	#####	2,070	1,800	10,200	3,160		170	3,100	22,000	58	0.9	37,800	0.8
	Avg	6/9/1999	1,220	955	2,570	131	ND	126	1,070	8,710	28	0.29	17,300	0.34
		Wells:		SC-A2A	SC-A3A	SC-A3B	SC-A4A	SC-A5A						
Seawater (Hem, 1989)			410	1,350	10,500	390	0	142	2,700	19,000	0.7	0.003	35,000	0.85

Averages ignore "non-detects" (ND); TDS = total dissolved solids.

Table 4-7
Groundwater Quality Summarized by Aquifer Zone

Flow Range (cfs)		Date	Stream- flow* (cfs)	Specific Conduc- tance (uS/cm)	pH	Cal- cium	Mag- nesium	So- dium	Pota- sium	Car- bonate	Bicar- bonate	Sul- fate	Chlo- ride	Nitrate (as N)	Iron	Man gane se	TDS		
						(mg/L)												Residue	Sum
						Soquel Creek at Soquel													
<10	N	83	83	83	42	35	34	83	35	42	83	19	83	1	1		9	10	
	Min	#####	0.1	661	7.7	69	20	15	1.3	0	208	75	44				435	442	
	Max	#####	9.9	1,000	8.7	83	28	73	6.8	17	264	117	106				502	494	
	Avg	#####	4.6	767	8.3	77	24	50	4.7	6.5	243	98	66	0.01	0.03		484	464	
10-40	N	38	38	38	15	19	19	38	20	15	38	9	38				2	6	
	Min	#####	10	575	8.2	63	16	30	2.9	0	182	91	25				421	365	
	Max	#####	32	797	8.7	84	25	58	5.5	20	262	132	70				475	420	
	Avg	#####	19	670	8.5	70	20	41	3.8	10	212	107	41				448	389	
40-100	N	15	15	15	5	8	8	15	8	5	15	1	15				1		
	Min	#####	41	416	8.1	44	11	10	2.6	0	126		14				383		
	Max	#####	84	630	8.5	72	18	35	3.6	7	209		44				383		
	Avg	#####	54	530	8.3	57	15	27	2.9	3.4	169	111	23				383		
>100	N	12	10	10	4	3	3	10	3	4	10		10						
	Min	#####	105	270	7.5	28	7.3	12	2.2	0	78		9.8						
	Max	4/9/1965	428	535	8.5	45	14	26	2.8	4	164		19						
	Avg	#####	207	398	8.0	39	11	20	2.4	1.0	125		14						
Brown & Caldwell,		#####	414	280	7.0	26	8.3	15	3.8	0	82	44	13	0.81	56	1.1	210		
		3/4/1981	30	550	7.7	55	19	34	6.0	0	166	91	35	0.41	14	0.2	386		
		West Branch Soquel Creek																	
		#####	0.73	625	7.6	53	25	55	5	0	260	48	70	0.08	0		433		
		Aptos Creek near Aptos																	
		#####	0.5	900	7.8	72	37	110	5.6	0	350	100	110	0.09	0		645		
		Aptos Creek at Aptos																	
		#####	0.4	1,080	7.9	73	38	86	5.5	0	350	91	100	0.14	0		604		

*Instantaneous flows, except for the two 1981 samples which are mean daily flows reported by USGS.

TDS = total dissolved solids

Source: <http://nwis.waterdata.usgs.gov/ca/nwis/qwdata>, except as noted.

Table 4-8
Soquel-Aptos Surface Water Quality

Source	No.	Total Dis-solved Solids	Major Cations				Major Anions				Sum Cat-ions	Sum An-ions	Total	Major Cations				Major Anions				Water Type
			Cal-cium (Ca)	Magne-sium (Mg)	So-dium (Na)	Potas-sium (K)	Car-bonate (CO ₃)	Bicar-bonate (HCO ₃)	Sul-fate (SO ₄)	Chlor-ide (Cl)				Cal-cium (Ca)	Magne-sium (Mg)	So-dium (Na)	Potas-sium (K)	Car-bonate (CO ₃)	Bicar-bonate (HCO ₃)	Sul-fate (SO ₄)	Chlor-ide (Cl)	
Production Wells	Wells	(mg/L)	(meq/L)											Percent of Cations				Percent of Anions				
Beltz wells (AA,A)*	6	430	3.6	1.5	0.87	0.19	0.00	2.1	1.2	1.6	6.2	5.0	11	58%	25%	14%	3%	0%	43%	25%	33%	Mixed Calcium
Main Street well (AA,Tu)	1	330	2.1	1.3	1.5	0.14	0.00	2.8	1.0	0.57	5.1	4.4	9.5	42%	27%	29%	3%	0%	64%	23%	13%	Mixed Bicarbonate
Service Area I wells** (AA,A)	~6	550	5.3	2.5	1.9	0.17	0.24	3.4	2.7	1.8	9.9	8.1	18	53%	25%	20%	2%	3%	42%	33%	22%	Mixed Calcium
Service Area II wells (A,BC,DEF)	5	430	2.1	2.5	3.0	0.14	1.1	4.0	1.4	1.2	7.9	7.7	16	27%	32%	39%	2%	14%	52%	18%	16%	Mixed Bicarbonate
Old Seacliff wells (DEF)	5	400	3.0	5.1	1.8	0.11	0.48	4.6	1.2	1.5	9.9	7.8	18	30%	51%	18%	1%	6%	59%	15%	20%	Magnesium-Bicarbonate
Service Areas III & IV wells (Qa/F)	6	250	1.6	2.2	0.81	0.07	0.00	2.3	0.42	0.58	4.6	3.3	8.0	34%	47%	17%	1%	0%	70%	13%	18%	Mixed Bicarbonate
Aquifer (monitoring wells)																						
Tp-AA (SC-10AA)	1	220	1.9	1.1	0.51	0.10	0.00	2.5	0.22	0.29	3.6	3.1	6.7	52%	31%	14%	3%	0%	83%	7%	9%	Calcium-Bicarbonate
Tp-A	6	410	2.4	1.1	3.2	0.11	2.4	3.0	1.9	1.0	6.8	8.3	15	35%	16%	47%	2%	29%	36%	23%	12%	Mixed
Tp-B (includes aquitard)	4	460	1.2	0.85	5.5	0.08	0.26	2.6	2.7	1.5	7.6	7.0	15	15%	11%	72%	1%	4%	37%	39%	21%	Mixed Sodium
Tp-C	4	480	2.5	1.9	3.9	0.12	0.25	3.4	2.2	1.7	8.4	7.5	16	30%	23%	46%	1%	3%	45%	29%	22%	Mixed Sodium Bicarbonate
Tp-D (includes aquitard)	2	360	0.86	1.2	4.2	0.09	0.27	3.3	0.82	0.99	6.3	5.4	12	14%	19%	66%	1%	5%	61%	15%	18%	Sodium-Bicarbonate
Tp-E	2	420	2.3	2.4	2.2	0.11	0.06	3.3	2.0	1.1	7.0	6.4	13	33%	35%	31%	2%	1%	51%	31%	17%	Mixed Bicarbonate
Tp-F (SC-8F, saline)	1	5,000	21	23	28	1.0	0.00	1.0	4.8	70	73	76	149	29%	32%	38%	1%	0%	1%	6%	92%	Mixed chloride
Qa/F (not intruded)	9	270	1.5	1.7	1.0	0.08	0.17	2.4	0.52	0.76	4.3	3.8	8.1	36%	39%	24%	2%	4%	62%	14%	20%	Mixed Bicarbonate
Qa/F (transitional)	4	480	2.5	2.9	1.8	0.08	0.00	2.3	1.8	2.8	7.3	6.9	14	34%	40%	25%	1%	0%	33%	26%	41%	Mixed
Qa/F (intruded)	5	17,000	61	79	112	3.3	0.00	2.1	22	246	255	270	525	24%	31%	44%	1%	0%	1%	8%	91%	Mixed Chloride
Seawater (Hem, 1989)		35,000	20	111	457	10.0	0.00	2.3	56	536	598	595	1,193	3%	19%	76%	2%	0%	0%	9%	90%	Sodium-Chloride
Stream																						
Soquel Creek at Soquel (cfs)																						
<10		480	3.9	1.9	2.2	0.12	0.22	4.0	2.0	1.9	8.1	8.1	16	48%	24%	27%	1%	3%	49%	25%	23%	Calcium-Bicarbonate
10-40		450	3.5	1.7	1.8	0.10	0.33	3.5	2.2	1.2	7.0	7.2	14	50%	23%	25%	1%	5%	48%	31%	16%	Calcium-Bicarbonate
40-100		380	2.8	1.3	1.2	0.07	0.11	2.8	2.3	0.66	5.4	5.8	11	53%	24%	22%	1%	2%	47%	40%	11%	Calcium-Bicarbonate
>100		250	1.9	0.94	0.85	0.06	0.03	2.1	1.5	0.41	3.8	4.0	7.8	51%	25%	22%	2%	1%	52%	37%	10%	Calcium-Bicarbonate
West Branch Soquel Creek (<1 cfs)		430	2.6	2.1	2.4	0.13	0.00	4.3	1.0	2.0	7.2	7.2	14	37%	28%	33%	2%	0%	59%	14%	27%	Mixed Bicarbonate
Aptos Creek near Aptos (<1 cfs)		650	3.6	3.0	4.8	0.14	0.00	5.7	2.1	3.1	12	11	22	31%	26%	41%	1%	0%	53%	19%	28%	Mixed Bicarbonate
Aptos Creek at Aptos (<1 cfs)		600	3.6	3.1	3.7	0.14	0.00	5.7	1.9	2.8	11	10	21	34%	29%	35%	1%	0%	55%	18%	27%	Mixed Bicarbonate

*Alkalinity used as an estimate of bicarbonate.

**Except Main St. well.

Shading indicates the dominant cations and anions that define the water type.

Table 4-9
Soquel-Aptos Water Quality Types

Author subarea user	Total Through- flow \cong Total Recharge	"Aquifer Yield" \cong Onshore Discharge	Native Out-flow to Ocean	Offshore Discharge Needed to Prevent Seawater Intrusion	Recharge Rate and Area		"Potential", "Safe", "Sustainable", "Practical Developable" Yield
					Average Rate	Area	
	(ac-ft/yr)				(in/yr)	(mi. ²)	(ac-ft/yr)
Hickey, 1968 primary Purisima aquifers	10,000 <i>a</i>				4	46	
M. Johnson, 1980 North of Zayante fault					5.6 4 - 7.2		
Muir, 1980 Purisima							4,100 to 4,400 <i>b</i>
Aromas							1,500 <i>c</i>
Total						50	5,900
Thorup, 1981 Purisima (& Aromas?)	12,670	10,200 to 11,600		1,200 to 2,400	4.6	51	8,000
LSCE, 1984a Purisima			>9,500				12,000 to 13,000
UCSC grad students, 1985 Purisima	10,475	9,975	500				
LSCE, 1987, 1990 Aromas			>12,000				
Essaid, 1992 Purisima concep. model (Table 5-4)	6,000 to 17,000				2 - 9	?	
numerical model (Fig. 5-3)	13,000	12,000	1,000			?	
Montgomery-Watson, 1998 Purisima & Aromas concep. model (Table 5-5) areal recharge					6.1	64	
num. model (Table 5-6) areal recharge	20,000				5.9	64	
boundary inflow	2,600						
Montgomery-Watson, 1999 Purisima							
SCWD							3,070 <i>d</i>
Other							3,160
Total							6,230
LSCE, 1997, 2004; SCWD, 1998 Aromas SCWD							1,800 <i>e</i>
This Study (Table 5-12) Purisima	12,200				4.4	52	
Aromas	3,600				4.7	14	
Total	15,800				4.5	66	

Notes

This table summarizes a wide variety of estimates and approaches. See Sec. 5.2 for further explanation.

Italics indicate values inferred from provided information.

(a) Discharge from "primary water bearing units" only.

(b) Estimated from 1962-74 average annual pumpage and pumpage corresponding to zero change in water level.

(c) Estimated from 1966-77 average annual pumpage and pumpage corresponding to zero change in water level.

(d) Based on prevention of saltwater intrusion given current well configuration and recommended reduced pumping from selected wells.

(e) Applies to existing SCWD wellfield only.

Table 5-1

Summary of Previous and Current Estimates of Groundwater Yield

Author	Producer	Period Groundwater Production			On-Shore Discharge (non-pumping)		Offshore Discharge (Outflow to Ocean)		"Potential", "Safe", "Sustainable", "Practical Developable" Yield			"Over- draft"
		Purisima	Aromas	Total	Purisima	Aromas	Purisima	Aromas	Purisima	Aromas	Total	
		(ac-ft/yr)										
Hickey, 1968	Total	<u>1966</u> 3,300										
Muir, 1980	SCWD	<u>1974</u> 2,820	<u>1,977</u> 400	<u>1974-77</u> 3,220								
	Beltz	420		420								
	CWD	106	44	150								
	Other	2,050	1,160	3,210								
	Total	5,400	1,600	7,000					4,100 to 4,400 <i>a</i>			1,000
										1,500 <i>b</i>		100
										5,900	1,100	
Thorup, 1981 (& Aromas?)	SCWD	<u>1974-80</u> 2,940										
	Beltz	330										
	CWD	130										
	Other	2,200										
	Total	5,600							8,000			0
LSCE, 1984	SCWD	<u>1983</u> 3,350										
	Other	<1,000										
	Total	<4,400										
							9,500		12,000 to 13,000			0
LSCE, 1987, 1990	SCWD		<u>1986-89</u> ~1,900									
							12,000		>1,900			0
Essaid, 1992 (see Figure 5-2)	Total	<u>1984</u> 3,600 <i>c</i>			10,600		400					
LSCE, 1994	Total	<u>1990</u> 11,400 <i>d</i>									~11,400	0
	"locally" <i>e</i>											>0
Montgomery-Watson, 1998 (see Table 5-6)	Total	<u>1982-93</u> 17,650			5,450		1,700					
Montgomery-Watson, 1999	SCWD	<u>~1992-99</u> 3,680								3,070 <i>f</i>		
	Other	3,160								3,160		
	Total	6,840								6,230		610
LSCE, 1997, 2004; SCWD, 1998	SCWD	<u>1997-2003</u> 2,100								1,800 <i>g</i>		~300 <i>g</i>
Wolcott, 1999; Pingree, 1997; Faler, 1992 and This Study (see Tables 5-7 and 5-11)		<u>1990s</u> Total Production										
	SCWD	3,800	2,200	6,000								
	Beltz	570	0	570								
	CWD	140	480	620								
	Other	2,200	900	3,100								
	Total	6,700	3,600	10,300								
		Consumptive Use										
	SCWD	3,550	2,060	5,600								
	Beltz	540	0	540								
	CWD	140	180	330								
	Other	1,500	560	2,000								
	Total	5,700		8,500	6,100		400					>0?
		2,800				700		0			>0	

Notes

This table summarizes a wide variety of estimates and approaches. There is some redundancy with Table 5-1. See Section 5.2 for further explanation.

Italics indicate values inferred from provided information. Sums may reflect small roundoff errors.

(a) Estimated from 1962-74 average annual pumpage and pumpage corresponding to zero change in water level.

(b) Estimated from 1966-74 average annual pumpage and pumpage corresponding to zero change in water level.

(c) Modeled SCWD production only.

(d) Based on water use estimates by Faler (1992).

(e) LSCE, 1994, p. 40.

(f) Given current well configuration and recommended reductions in selected wells.

(g) Applies to existing SCWD wellfield only.

Table 5-2
Summary of Previous Estimates of Developed Groundwater Conditions

Watershed	Rain- fall	Run- off	Evapotrans- piration	Recharge
	(in/yr)			
Soquel Creek	43.9	13.9	22.8 - 25.9	4.0 - 7.1
Aptos Creek	39.3	12.0	20.0 - 22.9	4.0 - 6.8
Corralitos Creek	37.9	10.9	19.7 - 22.3	4.6 - 7.2
Total	41.5	12.9	21.6 - 24.5	4.2 - 7.1
Average			23.1	5.6

Table 5-3
Estimated Water Budget North of Zayante Fault
(adapted from Johnson, M., 1980)

Watershed	Watershed Area		Estimate No. 1						Estimate No. 2 ^a				Comments
			Reported Unit Rates (ET estimated from 1953 Pajaro Valley study)			Estimated Recharge		Implied Area	ET Est. as 55% of Precip.	Estimated Recharge		Implied Area	
	Upstream of USGS Gage	Reported Portion in Essaid Model	Precip- itation	"Run- off" ^{nb}	ET	Unit Rate from Balance of Terms ^c	Reported Volu- metric Rate		ET	Unit Rate from Balance of Terms ^c	Reported Volu- metric Rate		
	(mi ²)			(in/yr)			(ac-ft/yr)	(mi2)	(in/yr)		(ac-ft/yr)	(mi2)	
Soquel Creek at Soquel	40.2	13.6	40.2	13.4	24.4	2.4	3,320	26.4	22.0	4.8	6,900	27.2	Recharge volume based on 27-mi ² area of uncertain significance.
West Branch Soquel Ck	12.2	4.5	44.1	15.5	25.6	3.0	1,890	11.8	24.2	4.4	2,810	12.1	Recharge volume based on entire watershed, not the portion within the model area.
Aptos Creek	12.2	6.5	36.0	9.4	23.2	3.3	2,200	12.3	19.8	6.7	4,350	12.1	
Branciforte Creek	17.3	10.3	39.0	14.6	24.1	0.3	280	16.7	21.5	2.9	2,810	18.1	
Total	81.9	34.9					7,700	67.2			16,900	69.4	Large disparity between unit and volumetric rates depending on area applied to.
Average Rate	Total Volumetric Rate/Total Implied Area					2.1				4.7			
	Unit Rates Weighted by Gaged Areas					2.2				4.6			
	Unit Rates Weighted by Model Areas					2.0				4.5			
	Total Volumetric Rate/Modeled Area					4.1				9.1			

^aUses same values of precipitation and runoff as Estimate No. 1. Differences in "implied area" probably due to roundoff error.

^bAlthough referred to as "runoff," this represents total gaged flow, which includes baseflow, which is derived from recharge, which thus should not be used to estimate recharge.

^cRecharge = Precipitation - Runoff - ET

Watershed	Watershed Area		Estimated Mean Annual Baseflow						Comments
	Upstream of USGS Gage	Reported Portion in Essaid Model	Gaged Area			Model Area			
			Reported	Unit	(in/yr)	Reported	Unit	(in/yr)	
			Volumetric Rate*	Rate		Volumetric Rate	Rate		
	(mi ²)		(cfs)	(ac-ft/yr)		(cfs)	(ac-ft/yr)		
Soquel Creek at Soquel	40.2	13.6	13.1	9,460	4.4	4.2	3,070	4.2	Using baseflow as an estimate of total recharge ignores groundwater discharge to wells and ocean.
West Branch Soquel Ck	12.2	4.5	3.2	2,300	3.5	1.1	770	3.2	
Aptos Creek	12.2	6.5	3.5	2,560	3.9	1.8	1,280	3.7	
Branciforte Creek	17.3	10.3	2.5	1,790	1.9	1.4	1,020	1.9	
Total	81.9	34.9	22.2	16,100		8.5	6,100		
Weighted Average					3.7			3.3	

*Baseflow estimated by "simple straight-line hydrograph separation."

Reported values originally in metric units (km², mm/yr, m³/sec)

Italics indicate values inferred from provided information.

Bold values are provided as estimates of basin throughflow.

None of the above estimates accounts for recharge in the Arana, Rodeo, Porter, or Valencia creek watersheds, or along the coastal terrace.

Table 5-4
USGS Conceptual Model
Estimate of Soquel-Aptos
Groundwater Throughflow
(Essaid, 1992)

IGSM Subregions Comprising Current Study Area ^a	Area		As Reported								Recharge Estimated as Balance of Reported Terms ^d		
			Precip.	Irrigation/ Water Use		ET	Precip.	Irrig. Runoff ^e	Recharge		Rate	Error?	Volume
	(mi ²)	(acres)		(in/yr)	(ac-ft/yr)		(in/yr)		(ac-ft/yr)	(in/yr)			
Agricultural Land													
1 Live Oak		76	30.0	27.8	176	34.1	17.1	0.6	5.8	37	6.0	0.2	38
2 Service Areas I & II		400	29.3	28.6	953	34.2	10.4	0.6	12.6	420	12.7	0.1	423
3 Service Areas III & IV		269	22.9	25.1	563	30.6	3.8	1.3	12.2	273	12.3	0.1	276
4 Watersheds south of Zayante fault		1,708	35.6	26.0	3,701	32.2	14.4	0.5	14.6	2,078	14.5	-0.1	2,064
5 North of Zayante fault		19	38.3	27.2	43	32.9	11.8	0.5	20.5	32	20.3	-0.2	32
7 Aromas Hills (25%) ^b		353	25.0	24.9	732	30.0	11.8	0.6	6.5	191	7.5	1.0	220
Weighted Total	4.4	2,825	32.0	26.2	6,168	32.1	12.6	0.6	12.9	3,032	13.0	0.1	3,054
Non-Agricultural Developed Land													
1 Live Oak		3,653	29.1	14.3	4,353	14.2	18.0	0.0	3.2	974	11.2	8.0	3,409
2 Service Areas I & II		3,548	29.0	17.9	5,292	15.2	16.2	0.0	5.4	1,597	15.5	10.1	4,583
3 Service Areas III & IV		851	24.9	22.3	1,581	14.4	13.5	0.0	6.6	468	19.3	12.7	1,369
4 Watersheds south of Zayante fault		1,266	33.4	36.4	3,840	18.2	20.9	0.0	30.7	3,239	30.7	0.0	3,239
5 North of Zayante fault		9	39.0	29.6	22	16.6	25.0	0.0	27.0	20	27.0	0.0	20
7 Aromas Hills (25%) ^b		134	24.3	22.8	255	15.3	16.8	0.0	15.0	168	15.0	0.0	168
Weighted Total	14.8	9,461	29.2	19.5	15,344	15.1	17.3	0.0	8.2	6,465	16.2	8.0	12,788
Undeveloped Land													
1 Live Oak		497	29.3	0.0	0	21.2	7.5	0.0	0.6	25	0.6	0.0	25
2 Service Areas I & II		2,159	30.9	0.0	0	21.9	6.9	0.0	2.0	360	2.1	0.1	378
3 Service Areas III & IV		915	26.8	0.0	0	19.8	3.6	0.0	3.4	259	3.4	0.0	259
4 Watersheds south of Zayante fault		18,730	36.1	0.0	0	22.7	8.5	0.0	4.9	7,648	4.9	0.0	7,648
5 North of Zayante fault		4,833	39.4	0.0	0	22.9	9.6	0.0	6.9	2,779	6.9	0.0	2,779
7 Aromas Hills (25%) ^b		1,523	25.5	0.0	0	19.5	4.5	0.0	1.4	178	1.5	0.1	190
Weighted Total	44.8	28,657	35.3	0.0	0	22.4	8.2	0.0	4.7	11,249	4.7	0.0	11,279
Weighted Total													
1 Live Oak	6.6	4,226	29.1	12.9	4,529	15.4	16.7	0.0	2.9	1,036	9.9	6.9	3,472
2 Service Areas I & II	9.5	6,107	29.7	12.3	6,246	18.8	12.5	0.0	4.7	2,376	10.6	5.9	5,384
3 Service Areas III & IV	3.2	2,035	25.5	12.6	2,144	19.0	7.8	0.2	5.9	1,001	11.2	5.3	1,904
4 Watersheds south of Zayante fault	33.9	21,704	35.9	4.2	7,541	23.2	9.7	0.0	7.2	12,965	7.2	0.0	12,951
5 North of Zayante fault	7.6	4,861	39.4	0.2	65	22.9	9.6	0.0	7.0	2,832	7.0	0.0	2,831
7 Aromas Hills (25%) ^b	3.1	2,010	25.3	5.9	987	21.1	6.6	0.1	3.2	536	3.5	0.3	578
Weighted Total	64.0	40,943	33.7	6.3	21,512	21.4	10.6	0.0	6.1	20,746	7.9	1.9	27,120

^aExcluded IGSM subregions 6, 8, and most of 7 (a total of 48 mi²), which lie within or are tributary to Pajaro Valley.

^bAcreage adjusted to reflect that only about 25% of subregion 7 lies within current study area.

^cAppears to include most stream baseflow.

^dRecharge = (Precip. + Irrig.) - (ET + Runoff)

Shaded values seem anomalously high.

Italic values indicate apparent discrepancy.

Table 5-5
Soquel-Aptos IGSM Estimated Recharge, 1982-93 Average

(adapted from Montgomery Watson et al., 1998)

IGSM Subregions Comprising Current Study Area ^a	Area (acres)	As Reported							
		Recharge		Discharge to Stream ^b	Stream Perc.	Boundary Flow	Sub- boundary Flow	Pumping	Change in Storage
		(in/yr)	(ac-ft/yr)	(ac-ft/yr)					
1 Live Oak	4,226	2.9	1,021	1,490	0	295	-182	790	-1,146
2 Service Areas I & II	6,107	4.6	2,359	1,853	0	-3	3,169	6,209	-2,537
3 Service Areas III & IV	2,035	5.6	956	0	0	-68	-854	2,125	-2,092
4 Watersheds south of Zayante fault	21,704	6.9	12,496	79	0	1,619	-5,518	7,506	1,011
5 North of Zayante fault	4,861	6.5	2,631	2,023	0	664	-1,040	62	170
7 Aromas Hills (25%) ^c	2,010	3.1	525	0	160	18	302	954	51
9 Offshore next to subregions 1 & 2	-	-	-	-	-	-57	1,652	-	-
Total (64 mi ²)	40,943	5.9	19,988	5,445	160	2,468	-2,471	17,646	-4,543
Inferred ^d									
Inflow from outside study area				2,596					
Outflow to ocean				1,723					
Outflow to Pajaro Valley				854					

^a Excluded IGSM subregions 6, 8, and 75% of 7 (a total of 48 mi²), which lie within or are tributary to Pajaro Valley.

^b Groundwater discharge to stream baseflow appears to be only partially compensated for (e.g., seems low for subregion 4).

^c Approximately 25 percent of IGSM subregion 7 is within Soquel-Aptos study area.

^d Based on net boundary flows, thus these are minimum values.

Table 5-6
Soquel-Aptos IGSM Simulated Groundwater Budget, 1982-93 Average
(adapted from Montgomery Watson et al., 1998)

User	Purisima (Wocott, 1999; and this study)											Aromas (Faler, 1992; and this study)											Total Water Use	Total Con- sump- tive Use	Total Return Flow	Comments		
	No. of Devel- oped Parcels	No. of Active Wells	Total Water Use (ac-ft/yr)	Consumptive Use (ac-ft/yr)							Retrun Flow (ac- ft/yr)	No. of Active Wells	Total Water Use (ac-ft/yr)	Consumptive Use (ac-ft/yr)							Retrun Flow (ac- ft/yr)							
				Indoor			Outdoor							Indoor			Outdoor											
				% of use	% lost	Sub- total	% of use	% lost	Sub- total					Total	% of use	% lost	Sub- total	Total										
Private Parcels																												
Urban																												
Residential and Commercial	217	200	124	70%	100%	87	30%	80%	30	117	7											124	117	7	may include stream diversions.			
Agriculture	17	21	93	0%	0%	0	100%	80%	74	74	19											93	74	19				
Seascape Golf Course	8		232	0%	0%	0	100%	80%	186	186	46											232	186	46				
Rural																												
Residential and Commercial	2,223	700	1,099	50%	25%	137	50%	80%	440	577	522	-	557	50%	25%	70	50%	80%	223	292	265	1,656	869	787	Aromas estimates from tables below.			
Agriculture	42	48	163	0%	0%	0	100%	80%	130	130	33	-	309	0%	0%	0	100%	80%	247	247	62	472	378	94				
Small Water System:																												
Cabrillo College indoor	5	3	200	100%	100%	200	0%	0%	0	200	0											200	200	0				
outdoor			85	0%	0%	0	100%	80%	68	68	17											85	68	17				
Other Urban	68	4	29	70%	100%	20	30%	80%	7	27	2											29	27	2				
Rural	325	23	211	50%	25%	26	50%	80%	84	111	100	-	58	50%	25%	7	50%	80%	23	30	27	269	141	128	Aromas est. from tables below.			
Central Water Distric	799	2	143	50%	100%	72	50%	100%	72	143	0	3	479	50%	25%	60	50%	80%	192	184	295	622	327	295	1997 use.			
City of Santa Cruz Beltz Well	-	3	574	70%	100%	402	30%	80%	138	540	34		0							0	0	574	540	34	2000 use.			
Soquel Creek Water Distric	-	11	3,780	70%	100%	2,646	30%	80%	907	3,553	227	6	2,193	70%	100%	1,535	30%	80%	526	2,061	132	5,973	5,615	358	Purisima 1997; Aromas 2002.			
Total non-SCWD			2,953							2,173	780		1,403							754	649	4,356	2,926	1,430				
Total			6,733							5,726	1,007		3,596							2,815	781	10,329	8,541	1,788				

Aromas Study Area Small Water Systems Compiled by Faler (1992) ^a	No. Connections	Water Use Factor	Total Use (ac-ft/yr)
Aptos Hills Mutual	18	0.442	8
Calabasas Rd Mutual	7	0.442	3
East Bel Mar Drive Water	6	0.442	3
Emerald City Water Co.	12	0.442	5
Freedom Mutual	3	0.442	1
Larkin Valley Ridge	5	0.442	2
Milky Way Mutual	10	0.442	4
Senda Ladera Mutual	5	0.442	2
Spring Valley Water	8	0.442	4
White Calabasas Mutual	11	0.442	5
Aptos High School			11
Aptos Ridge Mutual	13	0.442	6
Rancho Aptos Subdivision			2
Renaissance High School			2
Total	98		58

Aromas Study Area Parcel Water Use Compiled by Faler (1992) ^b								
Use Code	No. of Parcels					Total	Water Use Factor	Total Use (ac-ft/yr)
	APN Zone No.							
	45	46	49	107	108			
none		2	3			5	0.5	3
res 010-041		3	8			11	0.5	6
res 050-054		7	9			16	-	14
res 060-062		20	101		1	122	1	122
res 063-065			4			4	0.442	2
store 120			1			1	1	1
res 511	1	1	5			7	-	409
830			1			1	1	1
Total (non-ag)	1	33	132	0	1	167		557
nurseries 261		2	5			7	-	116
orchards 400		4	6			10	-	193
Ag Total		5	11			16		309

^aExcludes parcels and water systems southeast of Manresa Beach.

^bExclusive of parcels served by small water systems.

Summary	(mi ²)	Total Use		Consumptive Use		Return Flow	
		(ac-ft/yr)	(in/yr)	(ac-ft/yr)	(in/yr)	(ac-ft/yr)	(in/yr)
Approx. urban (mostly sewerd)	16	7,300	8.6	6,800	8.0	480	0.6
Approx. rural (non-sewered)	50	3,000	1.1	1,700	0.6	1,300	0.5
SCWD Service Area	14	6,000	8.0	5,600	7.5	360	0.5
Purisima Area	51.6	6,700	2.4	5,700	2.1	1,000	0.4
Aromas Area	14.4	3,600	4.7	2,800	3.7	780	1.0
Total Study Area	66.0	10,300	2.9	8,500	2.4	1,800	0.5

Table 5-7
Summary of Water Use Analysis by
Faler (1992), Pingree (1997), and Wolcott (1999)

This table reflects information compiled by the three cited studies, but uses only the most recent water-use factors (Wolcott, 1999).

Split between indoor and outdoor use is as assumed by Wolcott (1999) for rural areas and as reported by ESA (2004) for urban areas.

The bottom two tables provide an original tally of information compiled by Faler (1992) for the Aromas area, although applying Wolcott's water use factors.

SCWD groundwater production values are maximums, 1997 for Purisima wells and 2002 for Aromas wells.

The value of Beltz wellfield production is for 2000, the year of greatest use since 1990.

The groundwater production value for CWD is for 1997, its maximum year; all return flows are over Aromas.

WY	Soquel Creek									Aptos Creek		Branci- forte Ck	Santa Cruz Precipitation (NOAA)	
	USGS Gages					LKA Gages				USGS Gages		USGS at Santa Cruz		
	Soquel Creek At Soquel	West Branch	At Soquel minus West Br	Near Soquel	At minus Near	West Branch	"Upper" (East Branch)	West Br + Upper	At Soq minus WBr+Up	At Aptos	Near Aptos			
	(ac-ft/yr) (% avg)												(in/yr) (% avg)*	
1952	67,707 216%												44.58 147%	
1953	27,175 87%											11,763 24.41	80%	
1954	18,664 60%											6,019 23.84	79%	
1955	15,045 48%											7,499 23.88	79%	
1956	71,574 229%											26,380 39.67	131%	
1957	13,620 43%											4,715 22.19	73%	
1958	60,135 192%											28,324 50.09	165%	
1959	19,698 63%	6,999	12,699							3,733		11,498 24.77	82%	
1960	12,414 40%	3,698	8,716							3,169		8,111 21.43	71%	
1961	3,279 10%	1,649	1,630							991		3,358 17.78	59%	
1962	22,736 73%	7,222	15,514							4,129		12,120 27.47	91%	
1963	62,787 200%	22,941	39,846							14,537		19,948 33.74	111%	
1964	10,049 32%	3,604	6,445							2,637		4,895 19.03	63%	
1965	36,822 118%	11,352	25,470							6,721		13,823 30.64	101%	
1966	9,132 29%	3,275	5,857							1,527		5,312 20.48	67%	
1967	54,243 173%	17,889	36,354							10,301		23,541 40.00	132%	
1968	12,035 38%	5,183	6,852							2,613		6,770 21.46	71%	
1969	53,703 171%	20,301	33,402	53,855	-152					12,603		44.94 148%		
1970	44,516 142%	13,059	31,457	30,283	14,233					9,525		30.18 99%		
1971	22,665 72%	6,601	16,064	15,749	6,916					3,526		27.24 90%		
1972	6,162 20%	1,928	4,234	4,675	1,487					1,249	1,168	19.08 63%		
1973	50,745 162%										10,839	43.67 144%		
1974	46,846 150%										9,425	41.96 138%		
1975	25,517 81%										4,958	24.29 80%		
1976	3,304 11%										1,129	15.37 51%		
1977	2,094 7%										696	14.81 49%		
1978	39,591 126%										8,408	37.59 124%		
1979	16,411 52%										3,390	29.15 96%		
1980	38,173 122%										9,718	37.14 122%		
1981	9,786 31%										2,011	21.74 72%		
1982	66,193 211%										19,438	48.14 159%		
1983	122,608 391%										22,858	53.93 178%		
1984	24,785 79%										6,919	24.01 79%		
1985	12,900 41%					4,637					2,755	29.68 98%		
1986	64,481 206%					17,608						40.99 135%		
1987	7,628 24%					2,250						15.85 52%		
1988	4,896 16%					1,859	2,174	4,033	863			18.73 62%		
1989	12,972 41%					2,526	6,101	8,627	4,345			24.20 80%		
1990	7,812 25%					853	3,311	4,164	3,648			16.76 55%		
1991	9,604 31%					3,415	4,229	7,644	1,960			20.36 67%		
1992	13,912 44%					4,878	5,731	10,609	3,303			27.51 91%		
1993	39,726 127%					12,746	11,069	23,815	15,911			36.69 121%		
1994	6,936 22%					2,278	1,406	3,684	3,252			22.71 75%		
1995	56,271 180%					21,131	26,179	47,310	8,961			43.01 142%		
1996	42,651 136%					10,695	12,522	23,217	19,434			31.49 104%		
1997	53,857 172%					13,706	16,882	30,588	23,269			36.60 121%		
1998	63,691 203%					15,740	20,797	36,537	27,154			59.82 197%		
1999	34,224 109%					6,061	14,064	20,125	14,099			33.65 111%		
2000	41,362 132%					10,641	12,516	23,157	18,205			36.39 120%		
2001	16,816 54%					2,616	3,094	5,710	11,106			25.45 84%		
2002	17,508 56%					2,475	4,044	6,519	10,989			28.79 95%		
Avg	31,323 100%	8,979	17,467	26,141	5,621	7,562	9,608	17,049	11,100	5,519	7,408	12,130 30.34	100%	
Min	2,094 7%	1,649	1,630	4,675	-152	853	1,406	3,684	863	991	696	3,358 14.81	49%	
Max	122,608 391%	22,941	39,846	53,855	14,233	21,131	26,179	47,310	27,154	14,537	22,858	28,324 59.82	197%	
Period of Record % of Average*	100%	84%	84%	101%	101%	93%	90%	90%	90%	84%	106%	90%		
Adjusted Average		10,634	20,688	25,779	5,543	8,145	10,691	18,971	12,351	6,536	6,984	13,527		

*Based on Soquel Ck at Soquel record.

*Drought years in bold.

Heavy lines indicate boundaries between wet and dry periods.

Table 5-8
Gaged Water-Year Flows of Soquel, Aptos, and Branciforte Creeks

Station Name	Station	Gaged Flows							Estimated Baseflows											
		Period of Record							Soquel at	Adjusted	Adjusted	riod of Record		Soq. at	Adjusted	Adjusted	Adj. by			
		Re- ported (mi ²)	This Study	Who le Wate		No. of Whole WYs	Average Dis- charge	Unit Dis- charge				Estimated Average Baseflow ^a	Unit Base- flow				Adjusted Average Baseflow		Adjusted Avg. Unit Baseflow	
W Br Soquel Creek	LKA	8.9	8.8	1985 - 2002		18	7,560	16.08	92.8%	8,150	17.32	980	2.08	91.4%	1,070	2.28	1,060	2.24		
W Br Soquel Ck near Soquel	11159800	12.2	12.2	1959 - 1972		14	8,980	13.82	84.4%	10,630	16.37	1,940	2.99	92.6%	2,100	3.23	2,300	3.54		
Upper Soquel Creek	LKA	13.9	13.6	1988 - 2002		15	9,610	13.24	89.9%	10,690	14.73	890	1.22	91.7%	970	1.33	980	1.36		
Soquel Ck near Soquel	11159940	32.0	32.0	1969 - 1972		4	26,100	15.33	101.4%	25,800	15.11	4,840	2.84	98.5%	4,920	2.88	4,780	2.80		
Soquel Ck at Soquel	11160000	40.2	40.2	1952 - 2002		51	31,300	14.62	100.0%	31,300	14.62	5,620	2.62	100.0%	5,620	2.62	5,620	2.62		
Branciforte Ck at Santa Cruz	11161500	17.3	-	1953 - 1968		16	12,100	13.15	89.7%	13,500	14.66	1,780	1.93	102.6%	1,740	1.88	1,990	2.15		
Aptos Ck near Aptos	11159690	10.2	-	1972 - 1985		14	7,410	13.62	106.1%	6,980	12.84	1,470	2.70	100.4%	1,460	2.69	1,380	2.55		
Aptos Ck at Aptos	11159700	12.3	12.1	1959 - 1972		14	5,520	8.54	84.4%	6,540	10.12	1,270	1.97	92.6%	1,380	2.13	1,510	2.33		
*USGS station number or or Linsley, Kraeger & Assoc. station.				Average				13.55			14.47			2.29			2.38			
				Minimum				8.54				10.12			1.22			1.33		
				Maximum				16.08				17.32			2.99			3.23		

*USGS station number or
or Linsley, Kraeger & Assoc. station.

^aFrom Table 5-10.

Table 5-9
Unit Annual Flows and Estimated Unit Baseflows for Soquel, Aptos, and Branciforte Creeks

WY	Soquel Creek									Aptos Creek		Branci- forte Ck	Santa Cruz Precipitation (NOAA)		
	USGS Gages					LKA Gages				USGS Gages					
	Soquel Creek At Soquel		West Branch	<i>At Soquel minus West Br</i>	Near Soquel	<i>At minus Near</i>	West Branch	"Upper" (East Branch)	<i>West Br + Upper</i>	<i>At Soq minus WBr+Up</i>	At Aptos	Near Aptos	USGS at Santa Cruz		
	(ac-ft/yr)	(% avg)	(ac-ft/yr)										(in/yr)	(% avg)	
1952	8,862	158%											44.58	147%	
1953	8,121	144%										2,196	24.41	80%	
1954	5,960	106%										1,790	23.84	79%	
1955	5,449	97%										1,630	23.88	79%	
1956	8,216	146%										1,960	39.67	131%	
1957	5,456	97%										1,629	22.19	73%	
1958	8,346	148%										2,073	50.09	165%	
1959	4,830	86%	1,857	2,973						1,409		1,571	24.77	82%	
1960	4,678	83%	1,646	3,033						1,164		1,802	21.43	71%	
1961	2,472	44%	1,085	1,387						737		1,379	17.78	59%	
1962	3,822	68%	1,252	2,569						915		1,544	27.47	91%	
1963	8,689	155%	3,040	5,649						1,960		2,136	33.74	111%	
1964	4,408	78%	1,873	2,535						1,411		1,680	19.03	63%	
1965	6,309	112%	2,251	4,058						1,455		1,915	30.64	101%	
1966	4,197	75%	1,473	2,724						843		1,570	20.48	67%	
1967	6,952	124%	2,663	4,289						1,168		1,848	40.00	132%	
1968	4,352	77%	1,839	2,513						998		1,796	21.46	71%	
1969	7,684	137%	2,493	5,191	6,624	1,060				1,541			44.94	148%	
1970	6,338	113%	2,385	3,953	5,583	756				1,714			30.18	99%	
1971	5,179	92%	2,202	2,977	4,798	382				1,636			27.24	90%	
1972	2,938	52%	1,132	1,806	2,362	576				874	740		19.08	63%	
1973	5,997	107%									1,217		43.67	144%	
1974	7,516	134%									1,899		41.96	138%	
1975	6,093	108%									1,741		24.29	80%	
1976	2,410	43%									926		15.37	51%	
1977	1,496	27%									566		14.81	49%	
1978	5,113	91%									1,177		37.59	124%	
1979	4,003	71%									1,118		29.15	96%	
1980	5,911	105%									1,631		37.14	122%	
1981	3,151	56%									881		21.74	72%	
1982	8,036	143%									1,975		48.14	159%	
1983	14,235	253%									2,918		53.93	178%	
1984	7,424	132%									2,555		24.01	79%	
1985	4,666	83%					1,559				1,221		29.68	98%	
1986	6,933	123%					1,553						40.99	135%	
1987	3,137	56%					682	667	1,349	1,787			15.85	52%	
1988	1,955	35%					747	602	1,350	606			18.73	62%	
1989	2,303	41%					728	977	1,705	598			24.20	80%	
1990	3,842	68%					431	1,474	1,905	1,937			16.76	55%	
1991	2,032	36%					968	507	1,475	557			20.36	67%	
1992	2,538	45%					762	598	1,360	1,178			27.51	91%	
1993	4,448	79%					1,255	728	1,984	2,465			36.69	121%	
1994	2,290	41%					846	660	1,505	785			22.71	75%	
1995	8,192	146%					1,874	1,218	3,093	5,100			43.01	142%	
1996	6,748	120%					1,192	876	2,069	4,679			31.49	104%	
1997	7,168	128%					735	743	1,478	5,691			36.60	121%	
1998	10,433	186%					1,721	1,993	3,714	6,719			59.82	197%	
1999	8,201	146%					871	876	1,747	6,454			33.65	111%	
2000	6,845	122%					782	923	1,705	5,140			36.39	120%	
2001	5,113	91%					413	430	843	4,270			25.45	84%	
2002	5,177	92%					526						28.79	95%	
Avg	5,621	100%	1,942	3,261	4,842	693	980	885	1,819	3,198	1,273	1,469	1,782	30.34	100%
Min	1,496	27%	1,085	1,387	2,362	382	413	430	843	557	737	566	1,379	14.81	49%
Max	14,235	253%	3,040	5,649	6,624	1,060	1,874	1,993	3,714	6,719	1,960	2,918	2,196	59.82	197%
Period of Record % of Average*		100%	93%	93%	98%	98%	91%	92%	92%	92%	93%	100%	103%		
Adjusted Average			2,098	3,523	4,917	704	1,072	965	1,984	3,488	1,375	1,463	1,738		

*Based on Soquel Ck at Soquel record.

*Drought years in bold.

Heavy lines indicate boundaries between wet and dry periods.

Table 5-10
Estimated Water-Year Baseflows of Soquel, Aptos, and Branciforte Creeks

Watershed	Tp or Qa ^a	Drainage Area (mi ²)	Estimated Average Unit Rates (in/yr)								Estimated Volumetric Rates		
			Water- shed Precip. ^b	Total Stream Discharge		Stream Base- flow ^c	Storm Flow	Evapo- trans- piration (in/yr) ^d	Estimated Deep Recharge from Precip.	Estimated Precip. Recharge	Stream Baseflow	Estimated Deep Recharge from Precip.	Estimated Precip. Recharge
				Gaged ^c	Rainfall- Runoff Relation ^b								

Note: *Italics* indicate values with relatively more associated assumptions.

(Note: small roundoff errors)

This table represents a worksheet combining data, estimates, assumptions, and professional judgement for the purpose of arriving at the generalized estimates presented in Table 5-12.

^aIndicates values that contribute to the estimated recharge of either the Purisima study area (Tp; i.e., contributes groundwater to District Service Areas I & II) or the Aromas study area (Qa; i.e., contributes to District Service Areas III & IV).

^bEstimated from Figure 5-5, except for watersheds overlying the Aromas Formation, for which lower values are assumed due to the soil's high percolation capacity.

^cSee Table 5-9. Baseflows of ungaged streams (italics) estimated from a regression between Qb and Ppt for gaged streams: Qb = (0.07 x Ppt) -0.58.

^dEvapotranspiration estimated by: ET = (0.37 x Ppt)+10.4; slightly higher values assumed for fully forested areas, slightly lower values for Aromas areas. Phreatophyte ET is not explicitly accounted for. Regression equations for ET and Qb are assumed for the purpose of completing this table.

^e"Soquel Ck in study area" (mi²) = Soquel Ck at Soquel - ("West Branch Soquel Ck not in study area" + "Upper Soquel Ck not in study area")

^f"Aptos Ck in study area" (mi²) = Aptos Ck at Aptos - "Aptos Ck not in study area"

^gAssumes 10% of Valencia Ck recharge contributes to Aromas area.

Table does not account for return-flow recharge from "imported" water use in Live Oak area.

Table 5-11
Estimated Soquel-Aptos Baseflow
and Recharge by Watershed

Study Subarea	Area (mi ²)	Estimated Average Unit Rates (in/yr)			Estimated Volumetric Rates		
		Stream Baseflow	Deep Recharge from Precip.	Precipitation Recharge	Stream Baseflow	Deep Recharge from Precip.	Precipitation Recharge
		(in/yr)			(ac-ft/yr)		
Purisima North	7.4	2.4	2.3	4.7	950	910	1,850
Purisima Central	34.0	2.4	2.3	4.7	4,350	4,170	8,520
Coastal Terrace West	10.2	1.4	2.0	3.4	760	1,090	1,850
Purisima Average/Total	51.6	2.2	2.2	4.4	6,100	6,100	12,200
Aromas Sands	12.0	1.0	4.0	5.0	640	2,560	3,200
Coastal Terrace East	2.4	0.6	2.4	3.0	80	310	380
Aromas Average/Total	14.4	0.9	3.8	4.7	700	2,900	3,600
Average/Total	66.0	1.9	2.6	4.5	6,800	9,000	15,800

Based on unit rates estimated in Table 5-11.

Table 5-12

Estimated Soquel-Aptos Baseflow and Precipitation Recharge by Subarea

Table 7-1
Summary of Past Interpretations of Stream-Aquifer Interactions Along Soquel Creek

	General Approach	Concept and Method	Inherent Limitations	Investigators
1	Hydrogeology of creek alluvium and Purisima Formation.	The layering and texture of the alluvium and underlying Purisima Formation along Soquel Creek may include fine-grained layers capable of greatly impeding flow between the creek and the alluvium, or between the alluvium and the Purisima Formation. Borehole geologic and geophysical logs are used to investigate layering.	Borehole geology is not a direct measure of pumping effects on baseflow. At best, it can only be used to infer vertical permeability at a point. Vertical flow is governed by permeability over a wide area and also by the hydraulic gradient.	Todd Engineers, 2001; Balance Hydrologics, 2003.
2	Aquifer test of a well near the creek.	Look for break in slope (recharge boundary) or gradual deflection (leakiness) in a plot of drawdown versus time at an observation well near the pumping well. Also, measure streamflow upstream and downstream of the well before and during the test.	The short duration of typical aquifer tests (1 to 3 days) is not likely to detect gradual leakage at steady rates over years to decades.	Luhdorff & Scalmanini Consulting Engineers, 1991; Todd Engineers, 2001.
3	Comparison of stream and ground-water elevations along the length of the creek.	Water-level differences between the creek and nearby wells indicate the direction of seepage between the stream and aquifer.	The hydraulic gradient between the creek and adjacent shallow aquifer indicates only the direction of flow, not the rate of flow. If permeability is very low, seepage rates may be negligible.	Luhdorff & Scalmanini Consulting Engineers, 1985, 1998; and with Linsley, Kraeger Associates, 2003.
4	Mapping small streamflow gains and losses along the length of the creek.	If pumping induces stream infiltration, this seepage should be detectable as a decrease in surface flow near the well during low-flow periods. Flow is measured at numerous points along the creek while a well is operating. The flow gains or losses between measurement points are compared with the location and pumping rate of the well.	The accuracy of streamflow measurements is at best plus-or-minus about 5 percent. The expected range of potential streamflow depletion by District wells is 0 to 2 cfs, which means that their impact could not be reliably measured at flows greater than 40 cfs, or possibly less. Fortunately, all of the previous investigations focused their analysis on periods when flows were typically less than 10 cfs.	Linsley, Kraeger Associates, 1986; Balance Hydrologics, 2003.
5	Well versus stream water quality.	If the major-ion composition of well water is different from that of the stream, it may be from a different source.	Water quality changes as water percolates from the creek or land surface through the groundwater system. Dissolution and precipitation of minerals, cation exchange, adsorption and commingling with older water in the basin deposits can cause the relative and absolute concentrations of individual ions to change. These processes must be considered when drawing conclusions regarding differences in water quality.	Luhdorff & Scalmanini Consulting Engineers, 1991.

Table 7.1
Summary of Past Interpretations of Stream-Aquifer Interactions Along Soquel Creek (continued)

	General Approach	Concept and Method	Inherent Limitations	Investigators
6	Correlate normal streamflow fluctuations to possible causative factors.	Evaluating the magnitude and timing of short-term fluctuations in baseflow may suggest the relative importance of factors that affect it.	The magnitude of the flow fluctuations is within the plausible range of ET-related streamflow depletion along a 1 to 2 mile reach upstream of each gaging location. The flow fluctuations are too large to be attributable to private well pumping along the creek because most of that pumping is for domestic use, which is not strongly diurnal, and because pumping at wells more than a few hundred feet from the creek or more than a few miles upstream would cause flow depletions out of phase with the depletion from closer wells, which would diminish their combined effect to a magnitude smaller than the observed fluctuations.	Balance Hydrologics, 2003.
		If there is a strong correlation between annual groundwater pumping and summer baseflow, pumping is likely a significant factor affecting baseflow.	This method would fail to detect pumping effects if they are much smaller than effects caused by other factors.	Luhdorff & Scalmanini Consulting Engineers, Linsley, Kraeger Associates, 1998.
7	Correlate normal groundwater fluctuations with possible causative factors.	Comparing the timing and magnitude of observed fluctuations in groundwater levels with possible causes of those fluctuations (for example, pumping cycles, fluctuations in creek stage, or ET) can reveal which cause is dominant.	See detailed discussion in Appendix _.	Luhdorff & Scalmanini Consulting Engineers, Linsley, Kraeger Associates, 1998; 2003.
8	Comparison of baseflow trends with other streams unaffected by pumping.	The large effects of climate (wet and dry years) on baseflow can be filtered out of the flow dataset by comparing relative changes in baseflow trends between two nearby watersheds. Specifically, if baseflow in one stream changes from one period of years to a more recent period of years, while the average remained unchanged in a nearby stream, then the change at the first station must have been caused by something other than climatic conditions.	Watershed comparisons introduce new variables into the trend analysis, including: 1) differences in geology and storage response during long droughts, 2) differences in logging, grazing, fire and/or development history, and 3) differences in private well pumping upstream of the respective gages. Also, low flows are intrinsically difficult to gage accurately over extended periods because the stage-discharge relation can be significantly altered by in-channel vegetation growth, debris jams, or minor changes in bed topography.	Luhdorff & Scalmanini Consulting Engineers, Linsley, Kraeger Associates, 1998; Johnson, 2001.

Table 7.1
Summary of Past Interpretations of Stream-Aquifer Interactions Along Soquel Creek (continued)

	General Approach	Concept and Method	Inherent Limitations	Investigators
9	Comparison of average Soquel Creek baseflow and average rainfall for different periods.	By comparing average baseflow during hydrologically similar periods of years, changes in baseflow over time may be detectable.	Low flows are difficult to gage accurately. Apparent changes could reflect rating curve errors, or minor changes in vegetation or channel shape at the gage.	Luhdorff & Scalmanini Consulting Engineers, Linsley, Kraeger Associates, 1998; Todd Engineers, 2001.
10	Changes in the frequency distribution of low flows over time.	Evaluating the frequency distribution of low flows for different periods of time provides a more complete picture of the baseflow regime than average flows during those periods. The years selected for analysis can be stratified by climatic conditions (e.g. wet, normal, and dry years) to partially control for variability related to rainfall. Two methods can be used to evaluate frequency distributions. The first is to plot complete flow-duration curves, which involves ranking all the daily flows in each analysis period and plotting them against their percentile. The second is to select a small number of specific flow magnitudes (e.g. 0, 1, 2, 3 and 4 cfs) and plot the number of days in each analysis period that flows are less than or equal to those values.	As with all evaluations of low-flow records at gaging stations, those data are vulnerable to significant errors in the stage-discharge rating curve caused by minor changes over time in channel vegetation and bed form.	Jackson, 2001; Balance Hydrologics, 2003; this report (see Section 7.3).
11	Baseflow recession patterns.	The rate of dry-season baseflow recession could be a fairly sensitive indicator of pumping-related streamflow depletion. Comparing recession rates among various periods of years would reveal whether recession rates have changed over time.	Baseflow magnitude is strongly influence by annual rainfall, and a comparison among different years could lead to incorrect conclusions unless those years were climatically similar. Also, baseflow recession is affected by numerous factors including factors that also affect rainfall recharge. Thus, correctly identifying the cause of a change in recession rate may be difficult.	Johnson, 2001.

Table 7.1
Summary of Past Interpretations of Stream-Aquifer Interactions Along Soquel Creek (continued)

	General Approach	Concept and Method	Inherent Limitations	Investigators
12	Rainfall-runoff modeling.	Streamflow is strongly affected by rainfall. One of the ways to detect the effects of other factors is to evaluate changes in the relationship between rainfall and runoff. Methods of analysis include scatterplots and regression lines relating annual or seasonal streamflow to annual rainfall; multivariate regression models that relate current-month streamflow to weighted values of rainfall in a series of prior months (also known as the "antecedent precipitation index" method); and distributed-parameter computer models that simulate hydrologic processes such as interception, infiltration, depression storage, direct runoff, soil moisture storage, and interflow over short time intervals at a sub-watershed scale.	The fact that rainfall has a large effect on baseflow is an insufficient basis to conclude that other factors have little or no effect.	Luhdorff & Scalmanini Consulting Engineers, Linsley, Kraeger Associates, 1998; Jackson, 2001; Balance Hydrologics, 2003.
13	Groundwater modeling.	Creeks and rivers are often included in groundwater flow models as head-dependent boundary cells. Seepage to or from the creek is calculated during simulations as part of the overall groundwater flow system. During calibration, streambed permeability (conductance) is commonly calibrated so that simulated groundwater levels near the creek match measured water levels and the volume of seepage is consistent with the overall groundwater budget and flow patterns. Thus, groundwater modeling can be a useful tool for identifying gaining and losing reaches, estimating seepage rates, and investigating the effects of pumping on streamflow.	The modeling solution may not be unique. That is, equally good calibration results may be obtainable for various combinations of streambed conductance, aquifer transmissivity, and seepage flux.	Essaid, 1991; Montgomery Watson, Ali Taghavi & Associates, Luhdorff & Scalmanini Consulting Engineers, 1998.

	Water Year	Rainfall at Santa Cruz (inches)	Water Year	Soquel Creek Mean Annual Flow (cfs)
WET YEARS	1998	59.82	1983	169.4
	1983	53.93	1956	98.6
	1958	50.09	1952	93.3
	1982	48.14	1982	91.4
	1969	44.94	1986	89.1
	1952	44.58	1998	88.0
	1973	43.67	1963	86.7
	1995	43.01	1958	83.1
	1974	41.96	1995	77.7
	1986	40.99	1967	74.9
	1967	40.00	1997	74.4
	1956	39.67	1969	74.2
	1978	37.59	1973	70.1
NORMAL YEARS	1980	37.14	1974	64.7
	1993	36.69	1970	61.5
	1997	36.60	1996	58.8
	2000	36.39	2000	57.0
	1963	33.74	1993	54.9
	1999	33.65	1978	54.7
	1996	31.49	1980	52.6
	1965	30.64	1965	50.9
	1970	30.18	1999	47.3
	1985	29.68	1953	37.5
	1979	29.15	1975	35.2
	2002	28.79	1984	34.1
	1992	27.51	1962	31.4
	1962	27.47	1971	31.3
	1971	27.24	1959	27.2
	2001	25.45	1954	25.8
	1959	24.77	2002	24.2
	1953	24.41	2001	23.2
	1975	24.29	1979	22.7
	1989	24.20	1955	20.8
DRY YEARS	1984	24.01	1992	19.2
	1955	23.88	1957	18.8
	1954	23.84	1989	17.9
	1994	22.71	1985	17.8
	1957	22.19	1960	17.1
	1981	21.74	1968	16.6
	1968	21.46	1964	13.8
	1960	21.43	1981	13.5
	1966	20.48	1991	13.3
	1991	20.36	1966	12.6
	1972	19.08	1990	10.8
	1964	19.03	1987	10.5
	1988	18.73	1994	9.6
	1961	17.78	1972	8.5
	1990	16.76	1988	6.7
	1987	15.85	1976	4.6
	1976	15.37	1961	4.5
	1977	14.81	1977	2.9

Table 7-2
Classification of Water-Year Hydrologic Conditions